Diversion (DV)





Practice Description

A diversion is a watercourse constructed across a slope consisting of an excavated channel, a compacted ridge, or a combination of both. Most diversions are constructed by excavating a channel and using the excavated material to construct a ridge on the downslope side of the channel. Right-of-way diversions and temporary diversions are sometimes constructed by making a ridge, often called a berm, from fill material.

This practice applies to sites where stormwater runoff can be redirected to permanently protect structures or areas downslope from erosion, sediment, and excessive wetness or localized flooding. Diversions may be used to temporarily divert stormwater runoff to protect disturbed areas and slopes or to retain sediment on-site during construction.

Perimeter protection is sometimes diversions used at either the upslope or downslope side of a construction area.

Right-of-way diversions, sometimes referred to as water bars, are used to shorten the flow length on a sloping right-of-way and reduce the erosion potential of the stormwater runoff.

Perimeter protection is sometimes used to describe both permanent and temporary



Planning Considerations

Diversions are designed to intercept and carry excess water to a stable outlet.

Diversions can be useful tools for managing surface water flows and preventing soil erosion. On moderately sloping areas, they may be placed at intervals to trap and divert sheet flow before it has a chance to concentrate and cause rill and gully erosion. Simple water bars illustrate this concept (Figure DV-1).

Diversions may be placed at the top of cut or fill slopes to keep runoff from upgradient drainage areas off the slope. Diversions are also typically built at the base of steeper slopes to protect flatter developed areas that cannot withstand runoff water from outside areas. They can also be used to protect structures, parking lots, adjacent properties, and other special areas from flooding.

Diversions are preferable to other types of man-made stormwater conveyance systems because they more closely simulate natural flow patterns and characteristics. Flow velocities are generally kept to a minimum. When properly coordinated into the landscape design of a site, diversions can be visually pleasing as well as functional.

As with any earthen structure, it is very important to establish adequate vegetation as soon as possible after installation. It is usually important to stabilize the drainage area above the diversion so that sediment will not enter and accumulate in the diversion channel.

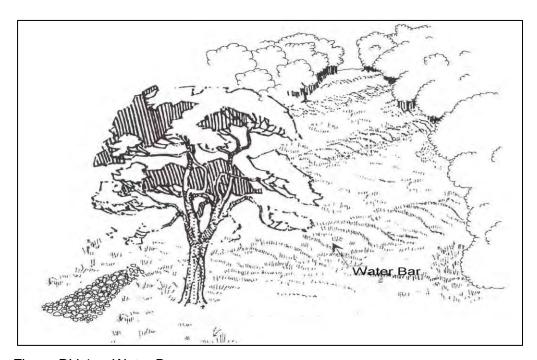


Figure DV-1 Water Bar

Design Considerations

Location

The location of the diversion should be determined by considering outlet conditions, topography, land use, soil type, length of slope, seepage (where seepage is a problem) and the development layout. Outlets must be stable after the diversion empties stormwater flow into it; therefore, care should be exercised in the location selection of the diversion and its outlet.

Capacity

The diversion channel must have a minimum capacity to carry the runoff expected from a storm frequency meeting the requirements of Table DV-1 with a freeboard of at least 0.3 foot (Figure DV-2).

The storm frequency should be used to determine the required channel capacity, Q (peak rate of runoff). The peak rate of runoff should be determined using the Natural Resources Conservation Service runoff curve number (RCN) method or other equivalent methods.

Table DV-1 Design Frequency

Diversion Type	Typical Area of Protection	24-Hour Design Storm
,,	71	Frequency
Temporary	Construction Areas	2-year
remporary	Building Sites	5-year
	Agricultural Land	10-year
	Mined Reclamation Area	10-year
Permanent	Recreation Areas	10-year
1 Cilianent	Isolated Buildings	25-year
	Urban areas, Residential, School,	50-year
	Industrial Areas, etc.	50-yeai

Diversions designed to protect homes, schools, industrial buildings, roads, parking lots, and comparable high-risk areas, and those designed to function in connection with other structures, should have sufficient capacity to carry peak runoff expected from a storm frequency consistent with the hazard involved.

Velocities

Diversions should be designed so that the design velocities are as high as will be safe for the planned type of protective vegetation and the expected maintenance, to minimize sediment deposition in the channel. Maximum permissible velocities are dependent upon the erosion resistance of the soil (Table DV-2) and the quality of the vegetation maintained.

Table DV-2 Permissible Velocities

		Velocity in Feet/Secon	d
Soil Texture	(Conditions of Vegetation	on
	Poor	Fair	Good
Sand, Silt, Sandy Loam, Silt Loam	1.5	2.0	3.0
Silty Clay Loam, Sandy Clay Loam	2.5	3.0	4.0
Clay	3.0	4.0	5.0

Channel Design

The diversion channel may be parabolic, trapezoidal or v-shaped, as shown in Figure DV-2 and should be designed in accordance with the procedure shown at the end of this practice. Land slope must be considered when choosing channel dimensions. On steeper slopes, narrow and deep channels may be required. On more gentle slopes, broad, shallow channels can be used to facilitate maintenance.

Ridge Design

The supporting ridge cross section should meet the configuration and requirements of Figure DV-2.

The side slopes should be no steeper than 2:1. Side slopes should be flatter, 5:1 to 10:1, when the diversion is to be permanent with mowing and other maintenance activities performed on or around it.

The width of the ridge at the design water elevation should be a minimum of 4 feet. The minimum freeboard should be 0.3 foot.

The design should include a 10% settlement factor.

Outlet

Diversions should have adequate outlets that will convey concentrated runoff without erosion. Acceptable outlets include practices such as *Grass Swale*, *Lined Swale*, *Drop Structure*, *Sediment Basin*, and *Stormwater Detention Basins*.

Stabilization

Unless otherwise stabilized, the ridge and channel should be seeded within 13 days of installation in accordance with the applicable seeding practice, *Permanent Seeding or Temporary Seeding*.

Disturbed areas draining into the diversion should be seeded and mulched prior to or at the time the diversion is constructed in accordance with the *Permanent Seeding*, *Temporary Seeding*, or *Mulching Practices* (whichever is applicable).

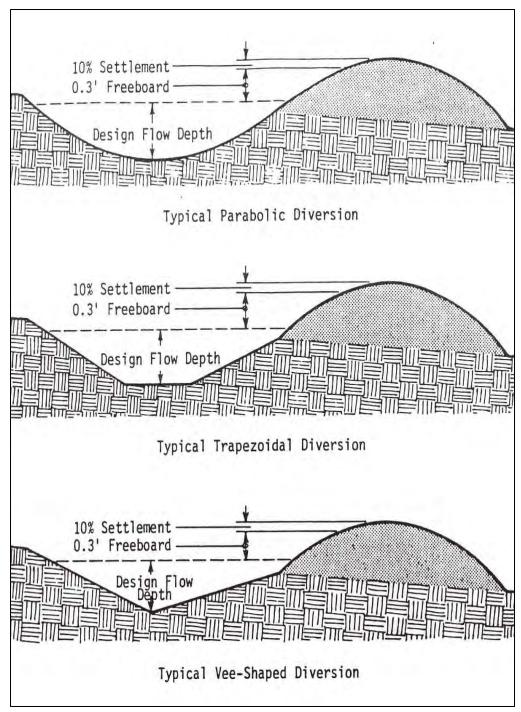


Figure DV-2 Typical Diversions Detail

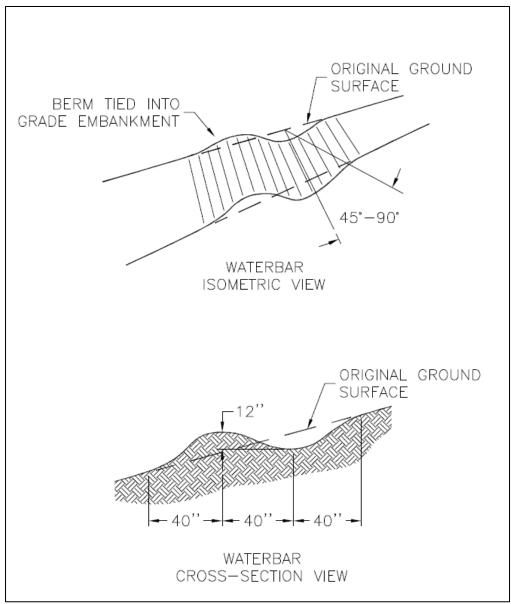


Figure DV-3 Water Bar Detail

Design Criteria

Tables DV-1 through DV-16 may be used to facilitate the design of grass-lined diversions with parabolic cross sections. These tables are based on a retardance of "D" (vegetation newly cut) to determine V_1 for stability considerations. To determine channel capacity, choose a retardance of "C" when proper maintenance is expected; otherwise, design channel capacity based on retardance "B." Refer to Table DV-2 for maximum permissible velocities. The permissible velocities guide the selection of V_1 and should not be exceeded. It is good practice to use a value for V_1 that is significantly less than the maximum allowable when choosing a design cross section. When velocities approach the

maximum allowable, flatter grades should be evaluated or a more erosion-resistant liner such as erosion control blanket or riprap should be considered. After the diversion dimensions are selected in the design tables, the top width should be increased by 4 feet and the depth by 0.3 foot for freeboard.

Example Problem

Given

Q: 30 cfs Grade: 1%

Soil: Sandy clay loam

Condition of vegetation expected: fair

Maintenance: low; will be cut only twice a year.

Site will allow a top width of 26 feet.

Find

Diversion top width and depth that will be stable and fit site conditions.

Solution

From Table DV-2, use maximum permissible velocity of 3.0 ft/sec.

Since maintenance will be low, use "B" retardance for capacity.

From Table DV-4, use retardance "D" and "B"; Grade 1.00 Percent Top width = 21.0 feet + 4 feet = 25.0 feet.

Depth = 1.6 feet + 0.3 foot = 1.9 feet.

 $V_2 = 1.3$ ft/sec.

Note: $V_1 < 3.0$ ft/sec.; Top width < 26 feet, design O.K.

Note: It is good practice to select a cross section that will give a velocity, V_I , well below the maximum allowable whenever site conditions permit. Wide, shallow cross sections are more stable and require less maintenance. It is always prudent to evaluate flatter design grades in order to best fit diversions to the site and keep velocities well below maximum allowable.

Table DV-3 Parabolic Diversion Design Chart (Retardance "D" and "B," Grade 0.50%)

Q	,	/1=2.0	1 1	1	/1=2.5		1	/1=3.0	1	1	/1=3.5		,	/1=4.0		,	V1=4.5		1	/1=5.0			V1=5.5			V1=6.0	
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30	21.0	2.0	1.0	13.9	2.3	1.4		-	-	- V	7	The state of	77		-		4-2-	7.	10000			-	-		-		
35	24.6	2.0	1.1	16.4	2.3	1.4	10.7	2.8	1.8			-	-					-				2					
40	28.5	2.0	1.0	18.9	2.3	1.4	12.6	2.7	1.8	-	75	100		-			-	1	-								
45	31.9	2.0	1.1	21.4	2.3	1.4	14.4	2.6	1.8		-	1			5							7-	3	1			
50	35.5	2.0	1.1	23.9	2.2	1.4	16.2	2.5	1.8	9.9	3.4	2.2			***	100	17	3 .		Cargo ve t							
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70	49.6	2.0	1.1	34.0	2.2	1.4	23.1	2.5	1.8	15.8	2.9	2.3	11.0	3.6	2.6	Arthur -		14. 14	dia es			dir as	ale co	1	1		2100
75	53.1	2.0	1.1	36.4	2.2	1.4	24.9	2.5	1.8	17.1	2.8	2.3	12.7	3.4	2.7					200		-80	V	Filters are			
80	56.6	2.0	1.1	38.8	2.2	1.4	26.6	2.5	1.8	18.4	2.8	2.3	13.7	3.3	2.7							1001					
85	60.2	2.0	1.1	41.2	2.2	1.4	28.3	2.5	1.8	19.7	2.8	2.3	14.8	3.2	2.7		/				144	1.30		N N			
90	63.7	2.0	1.1	43.6	2.2	1.4	30.0	2.4	1.8	20.9	2.8	2.3	15.9	3.2	2.7			1				A					
95	67.2	2.0	1.1	46.1	2.2	1.4	31.7	2.4	1.8	22.1	2.8	2.3	16.9	3.1	2.7			12.564						8			7-3
100	70.8	2.0	1,1	48.5	2.2	1.4	33.7	2.4	1.8	23.4	2.8	2.3	17.9	3.1	2.7	12.3	3.9	3.1	G. 7.								
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110	77.8	2.0	1.1	53.3	2.2	1.4	37.1	2.4	1.8	25.8	2.7	2.4	19.9	3.1	2.7	14.6	3.6	3.1	277				4	• •			1
115	81.4	2.0	1.1	55.7	2.2	1.4	38.7	2.4	1.8	27.0	2.7	2.4	20.8	3.0	2.7	15.4	3.6	3.1						- To	1		1
120	84.9	2.0	1.1	58.1	2.2	1.4	40.4	2.4	1.9	28.2	2.7	2.4	21.8	3.0	2,7	16.3	3.5	3.1	- W		4	-	war vision		4		1
125	88.4	2.0	1.1	60.6	2.2	1.4	42.1	2.4	1.9	29.4	2.7	2.4	22.8	3.0	2.7	17.1	3.5	3.1	- 10	16	F		\$124 to m	ulas est	4.	n.	
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135	95.5	2.0	1.1	65.4	2.2	1.4	45.4	2.4	1.9	31.8	2.7	2.4	24.8	3.0	2.7	18.7	3.4	3.2	10000							1	
140	99.0	2.0	1.1	67.8	2.2	1.4	47.1	2.4	1.9	33.1	2.7	2.4	25.7	3.0	2.8	19.4	3.4	3.2			8 1	15 30		200		17 -7	
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50	106.1	2.0	1.1	72.6	2.2	1.4	50.5	2.4	1.9	35.5	2.7	2.4	27.7	3.0	2.8	21.0	3.4	3.2	14.4	4.3	3.6			1		. 14.	-

Table DV-4 Parabolic Diversion Design Char (Retardance "D" and "B," Grade 1.00%)

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-																										
9.7	1.6	1.0	6.2	2.0	1.2																					
14.8	1.5	1.0	10.2	1.7	1.3	6.5	2.2	1.5																		
20.2	1.5	1.0	13.8	1.7	1.3	9.6	1.9	1.6																		
25.1	1.5	1.0	17.4	1.7	1.3	12.2	1.9	1.6	8.5	2.2	2.0															
30.1	1.5	1.0	21.0	1.6	1.3	14.9	1.8	1.7	10.6	2.1	2.1															
35.1	1.5	1.0	24.7	1.6	1.3	17.5	1.8	1.7	12.6	2.0	2.1	8.9	2.4	2.5												
40.1	1.5	1.0	28.2	1.6	1.3	20.0	1.8	1.7	14.5	2.0	2.1	10.5	2.3	2.5	7 3											
45.1	1.5	1.0	31.7	1.6	1.3	22.5	1.8	1.7	16.4	2.0	2.1	12.1	2.2	2.5	8.2	2.8	2.9									
50.2			35.2	1.6		25.4	1.8	1.7	18.3	2.0	2.1	13.6	2.2	2.5	10.0	2.6	2.9									
55.2	0.00			1.6		27.9	1.8	1.7	20.3	1.9	2.1	15.1	2.2	2.5	11.2	2.5	3.0									
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45.3	1.5	1.0	102.0	1.6	1.3	73.3	1.8	1.7	54.1	1.9	2.1	41.1	2.0	2.6	32.1	2.2	3.0	24.1	2.5	3.6	19.7	2.7	4.0	16.8	3.0	4
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1.6 1.3 30.4 1.8 1.7 22.2 1.9 2.1 10.5 2.1 12.5 1.0 2.6 14.8 2.4 3.0 10.6 2.8 3.5 1.5 1.0 43.3 1.6 1.3 38.0 1.8 1.7 24.0 1.9 2.1 18.0 2.1 2.5 12.4 2.4 3.0 10.6 2.8 3.5 1.5 1.0 43.3 1.6 1.3 38.0 1.8 1.7 2.0 1.9 2.1 1.8 1.7 2.2 2.1 2.5 1.2 2.5 12.4 2.4 3.0 10.6 2.8 3.5 1.5 1.0 43.3 1.6 1.3 38.0 1.8 1.7 2.0 1.9 2.1 2.2 2.2 2.5 1.2 2.5 12.4 2.4 3.0 10.6 2.8 3.5 1.5 1.0 43.3 1.6 1.3 38.0 1.8 1.7 2.5 1.9 1.9 2.1 2.2 2.5 1.5 1.0 4.2 3.1 1.5 2.8 3.5 1.5 1.0 4.5 3.5 1.6 1.3 38.0 1.8 1.7 3.9 1.9 2.1 2.2 2.5 1.5 1.0 4.2 3.3 1.1 4.4 2.6 3.6 1.9 3.1 3.5 1.5 1.0 4.5 3.1 1.5 1.0 4.5 3.1 1.5 1.0 4.5 3.1 1.5 1.0 4.5 3.1 1.5 1.0 4.5 3.1 1.5 1.0 4.5 3.1 1.5 1.0 4.5 3.1 1.5 1.0 4.5 3.1 1.5 1.0 4.5 3.1 1.5 1.0 4.5 3.1 1.5 1.0 4.5 3.1 1.5 1.0 4.5 3.1 1.5 1.0 4.5 3.1 1.5 1.0 4.5 3.1 1.5 1.0	9.7 1.6 1.0 6.2 2.0 1.2

Table DV-5 Parabolic Diversion Design Chart (Retardance "D" and "B," Grade 2.00%)

| V | 1=20 | 5 | 1 | n=2.5 | - | | /1=3.0 |
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 | 1=3.5 | | | /1=4.0 | | | 11-4.5 |
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 | D | Va | 7 | D | V2 | Ť | D | Va
 | 17 | D | V2 | 1
 | D | MS. | T | D | V2
 |
| 24 | | A CONTRACTOR | | - | 70 | 100 | |
 | -

 | | - | - | - Allen | | - | - |
 | | | | 7
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 |
| | 27.7 | A STATE OF THE PARTY OF | 9.5 | 13 | 12 | 70 | 14 | 13
 | -

 | - | -71 | 3 | | 200 | | - |
 | | - | 5 |
 | 200 | | - | |
 |
| | and the latest designation of the latest des | | | | | | | | 8.0

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 | 5.5 | 1.9 | 2.1 | | | | V-
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 | 5.3 | | \exists | |
| - | Contract of the | | The second second | | - | 14.6 | |
 | 10.9

 | 1.5 | 1.9 | 8.1 | 1.5 | 23 | 5.5 | 2.1 | 2.6
 | | | |
 | | | 100 | |
 |
| | - | _ | | | | 16.5 | | 1.5
 | 13.5

 | 1.4 | 1.0 | 10.4 | 1.6 | 2.3 | 7.9 | 1.5 | 2.7
 | 1 4 | | 1 |
 | 75 | | | 9,78 | 3.
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| | | _ | | | | 22.2 | | 1.6
 | 16.6

 | 54 | 1.9 | 12.7 | 1.5 | 23 | 9,7 | 1.7 | 2.7
 | 7.3 | 20 | 3.1 | -44.
 | 3.8 | - | | 7.5 |
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| 1.4 | | and the board | | | | 25.8 | 1.3 | 1.6
 | 19.6

 | 1.4 | 1,9 | 14,9 | 1.5 | 2.5 | 11.5 | 1.7 | 2.7
 | A CONTRACTOR | - | | - 740
 | 10.40 | 3.51 | 53 | 4 |
 |
| - | | 0.9 | 39.0 | | | 29.5 | 1.3 | 1.8
 | 22.4

 | 1.4 | 1.8 | 17.1 | 1.5 | 2.3 | 13.3 | 1.6 | 2.0
 | 10.4 | | |
 | | | 30.70 | 7 | 5
 |
| | | 0.9 | 43.9 | 1.2 | 1.2 | 33.2 | 1.3 | 1.0
 | 25.2

 | 1.4 | 1.9 | 19.3 | 1.5 | 2.3 | 15.0 | 1.5 | 2.8
 | 11.8 | 1.8 | | 100000
 | _ | | -1 | 100 | 100
 |
| | | 0.9 | 48.5 | 12 | 1.2 | 35.8 | 1.3 | 1.5
 | 26.0

 | 1.4 | 1.9 | 21,7 | 1.5 | 2.5 | 58.7 | 1.5 |
 | 13.2 | 1.8 | _ |
 | 4 | | and the second second | | 4
 |
| | | 0.9 | 53.6 | 1.2 | 12 | 40.5 | 1.3 | 1.6
 | 30.7

 | 1.4 | 1.9 | 23.9 | 1.5 | 2.3 | 18.5 | 1.6 | 2.8
 | 14.6 | | |
 | Annual Property | the second second | | | 4
 |
| 67.7 | | 0.9 | 58.5 | 1.2 | 1.2 | 44.2 | 1.3 | 1.5
 | 33.5

 | 1.4 | 1,9 | 26.0 | 1.5 | 2.3 | 20 Z | 1,8 | 2.6
 | 16.0 | 1.7 | |
 | 1,0 | | | | 4
 |
| 95.0 | 4.2 | 0.9 | 63.4 | 12 | 1.2 | 47.9 | 1.3 | 1.6
 | 36.3

 | 1.4 | 1.9 | 26,2 | 1.5 | 2.3 | 22,1 | 18 |
 | 17.4 | 1.7 | | _
 | - | | | - | 4
 |
| 102.3 | 1.2 | 0.9 | 86.2 | 1.2 | 12 | 51.6 | 1.5 | 1,6
 | 39.1

 | 1,4 | 1.9 | 30.3 | 1.5 | | 23.8 | 1.6 | 1.74
 | 18.8 | | |
 | | | | the latest street, where | 4
 |
| 109.6 | 1.2 | 0.9 | 73.1 | 1.2 | 1.2 | 55.2 | 1.3 | 1.6
 | 41.9

 | 1.4 | 1.9 | 32.5 | 1.5 | - | | 1.8 | and the last
 | 20.1 | | | _
 | - | | | - | 4
 |
| 116.9 | 1.2 | 0.9 | 78.0 | 1.2 | 12 | 68.9 | 1.3 | 1.6
 | 44.7

 | 1.4 | 1.9 | 34.5 | | | | 1.6 |
 | | | April 2 September 1 |
 | _ | 2 | | | 4
 |
| 124.2 | 12 | 69 | 82,5 | 1.2 | 12 | 62.6 | 1.3 | 1.6
 | 47.4

 | 1.4 | 1.9 | - A | 1.0 | _ | | 1.5 |
 | | | |
 | - | A STATE OF THE PARTY. | - Marine Company | | 4,
 |
| 131.5 | 1.2 | 0.9 | 87.7 | 12 | 1.2 | 65.3 | 1.3 | 1.6
 | 50.2

 | 1.4 | 1.9 | | 1.5 | | | A Company of the | ALC: UNKNOWN
 | No. of Concession, Name of Street, or other Designation, Name of Street, or other Designation, Name of Street, Original Property and Name of Stree | _ | | | The second second
 | | | | 4 |
| 136.5 | 1.2 | 0.9 | 92.6 | 1.2 | 1.2 | 69.9 | 1.3 | 1.6
 | 53.0

 | 1.4 | 1.9 | 4,444 | _ | | | - |
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 |
| 146.1 | 1.2 | 0.9 | 97.5 | 1.2 | 1.2 | 73.6 | 1.3 | 1,8
 | 55.5

 | 1.4 | 1.0 | 43.3 | 1.5 | A THE REAL PROPERTY. | | |
 | Supplement and | Service of the Control of the Contro | | | -
 | | The second second | | 4 |
| 153.4 | 12 | 0,9 | 102.3 | 12 | 1.2 | 77.3 | 1.3 | 1.6
 | 58.6

 | 1.4 | 1.9 | 45.4 | 1.5 | | | A condition to | _
 | | | |
 | All and the second | | | | 4
 |
| 180.7 | 1.2 | 0.9 | 107.2 | 1.2 | 1.2 | 81.0 | 1.3 | 1.5
 | 61.4

 | 1.4 | 1.9 | | _ | | | |
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| 188.0 | 1.2 | 0.9 | 112.1 | 1.2 | 1.2 | 64.7 | 1.3 | 1.8
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| 175.3 | 1.2 | 0.9 | 117.0 | | | 08.3 | 1.3 | 1.8
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| 182.5 | 1.2 | 0.9 | 121.0 | | | 92.0 | | 1.6
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 | | Annual Property | | _ | - | | |
 | | ALC: UNKNOWN | Name and | ACCRECATION AND PROPERTY.
 | Contract of | | | | 4
 |
| 169.9 | 12 | 0.9 | 126.7 | 1.2 | | 95.7 | | 1,6
 | A contractor

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 | | | | the lateral way | 4
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| 197.3 | 1.2 | 0.8 | 131.6 | | | | | The second second
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 | The second second | A Company of the Contract of t | 112 | | 14 |
| 204.6 | 1.2 | 0.9 | 136.5 | | 1,2 | 103.1 | 1.3 | 1.6
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 | | - | | | mineral residence | | |
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 | - | Section 1 | | - | -
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| 211.9 | 12 | 0.9 | 141.3 | 1.2 | 1.2 | 105.7 | 1.3 | 1.6
 |

 | 14 | - | and the latest division in the latest divisio | | | - | - | |
 | | - Company | |
 | - | - | Co. College | 4 |
| 219.2 | 1.2 | 0.9 | 145.2 | 1.2 | 1.2 | 110.4 | 13 | 1.8
 | 83.7

 | 1.4 | 1.9 | 64.9 | 1.5 | 23 | 50.9 | 1,0 | 2.5
 | 40.8 | 1.7 | 3.3 | 32.4
 | 1.0 | 3,1 | 41.0 | 1.0 | 1
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| | 7,1
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1.2 36.8 1.3 1.6 28.0 80.4 1.2 0.9 63.4 1.2 1.2 36.8 1.3 1.6 38.1 67.7 1.2 0.9 66.2 1.2 1.2 40.5 1.3 1.5 33.5 95.0 1.2 0.9 63.4 1.2 1.2 55.2 1.3 1.6 38.3 109.6 1.2 0.9 73.1 1.2 1.2 55.2 1.3 1.6 38.3 109.6 1.2 0.9 73.1 1.2 1.2 68.9 1.3 1.6 38.1 109.6 1.2 0.9 78.0 1.2 1.2 68.9 1.3 1.6 44.7 124.2 1.2 0.9 87.7 1.2 1.2 68.9 1.3 1.6 44.7 124.2 1.2 0.9 87.7 1.2 1.2 68.9 1.3 1.6 50.2 186.1 1.2 0.9 97.5 1.2 1.2 77.3 1.3 1.6 50.2 186.1 1.2 0.9 97.5 1.2 1.2 77.3 1.3 1.6 50.2 186.3 1.2 0.9 107.2 1.2 1.2 68.3 1.3 1.6 50.2 186.4 1.2 0.9 17.0 1.2 1.2 68.3 1.3 1.6 64.2 175.3 1.2 0.9 17.0 1.2 1.2 68.7 1.3 1.6 64.2 175.3 1.2 0.9 131.6 1.2 1.2 98.4 1.3 1.6 67.5 187.7 3 1.2 0.9 131.6 1.2 1.2 98.4 1.3 1.6 75.3 180.4 1.2 0.9 131.6 1.2 1.2 98.4 1.3 1.6 75.3 180.4 1.2 0.9 131.6 1.2 1.2 98.4 1.3 1.6 75.3 180.4 1.2 0.9 131.6 1.2 1.2 98.4 1.3 1.6 75.3 180.4 1.2 0.9 131.6 1.2 1.2 98.4 1.3 1.6 75.3 | T D V2 T D V2 T D V2 T D V2 T D V3 T D 7.1 1.2 0.9 9.5 1.3 1.2 7.0 1.4 1.5 22.0 1.2 0.9 14.5 1.3 1.2 10.0 1.4 1.5 8.0 1.5 29.3 1.2 0.9 19.6 1.2 1.2 14.8 1.3 1.5 10.9 1.5 38.6 1.2 0.9 24.4 1.2 1.2 10.5 1.3 1.5 13.8 1.4 43.9 1.2 0.9 34.2 1.2 1.2 22.2 1.3 1.6 16.6 1.4 58.5 1.2 0.9 34.2 1.2 1.2 22.8 1.3 1.6 16.6 1.4 58.5 1.2 0.9 34.0 1.2 1.2 22.5 1.3 1.6 16.6 1.4 58.5 1.2 0.9 43.8 1.2 1.2 23.5 1.3 1.6 22.4 1.4 65.8 1.2 0.9 43.8 1.2 1.2 33.2 1.3 1.6 25.2 1.4 72.1 1.2 0.9 43.8 1.2 1.2 33.8 1.3 1.6 25.2 1.4 80.4 1.2 0.9 63.8 1.2 1.2 40.5 1.3 1.5 30.7 1.4 67.7 1.2 0.9 63.8 1.2 1.2 40.5 1.3 1.5 30.7 1.4 67.7 1.2 0.9 63.4 1.2 1.2 55.8 1.3 1.6 39.1 1.4 69.0 1.2 0.9 63.4 1.2 1.2 55.2 1.3 1.6 39.1 1.4 109.6 1.2 0.9 63.4 1.2 1.2 55.2 1.3 1.6 39.1 1.4 109.6 1.2 0.9 73.0 1.2 1.2 55.2 1.3 1.6 39.1 1.4 109.6 1.2 0.9 78.0 1.2 1.2 55.2 1.3 1.6 39.1 1.4 109.6 1.2 0.9 67.7 1.2 1.2 68.3 1.3 1.6 50.2 1.4 109.6 1.2 0.9 78.0 1.2 1.2 68.3 1.3 1.6 50.2 1.4 109.6 1.2 0.9 67.7 1.2 1.2 68.3 1.3 1.6 50.2 1.4 109.6 1.2 0.9 78.0 1.2 1.2 77.3 1.5 1.6 39.1 1.4 109.7 1.2 0.9 102.3 1.2 1.2 88.9 1.3 1.6 64.2 1.4 109.8 1.2 0.9 102.3 1.2 1.2 77.3 1.5 1.6 58.6 1.4 109.7 1.2 0.9 102.3 1.2 1.2 89.4 1.3 1.6 64.2 1.4 109.7 1.2 0.9 102.3 1.2 1.2 98.4 1.3 1.6 64.2 1.4 109.7 1.2 0.9 121.8 1.2 1.2 98.4 1.3 1.6 72.5 1.4 109.7 1.2 0.9 131.6 1.2 1.2 98.4 1.3 1.5 75.3 1.4 109.7 1.2 0.9 131.6 1.2 1.2 98.4 1.3 1.5 75.3 1.4 | T D V2 7.1 1.2 0.9 | T D V2 T | T D V2 T | T D V2 7.1 1.2 0.9 | T D V2 T T D V2 D D V2 T D V2 D D D D D D D D D D D D D D D D D | T D V2 T | T D V2 T | T D V2 T | T D V2 T | T D V2 T | T D V2 T | T D V2 T | T D VZ T | T D V2 T | T D V2 T |

Table DV-6 Parabolic Diversion Design Chart (Retardance "D" and "B," Grade 4.00%)

CFE	1	71-2.0		- 4	/1=2.5		1	/1×3.0		-	/1<3.5		1	/1-4.0		173	1-4.6			1-6,0	(Cab	3	1=5.5	TIL	- 4	1-0.0	1
-	7	D	V2	T	D	V2	7	D	V2	+	D	V2	T	D	V2	T	D	V2	7	D	V2	T	0	V2	7	D	TV
5	10.1	0.0	0.8	7.0	1.0	1.1	4.0	1.1	1.4					1		1	100	-	-	-		200	77		-2-1	-	1
10	20.6	0.9	0.6	14.4	0.0	1.1	10.3	1.0	1.4	7.9	1.1	1.2	6.1	1.2	2.1	4.5	1.4	24		40.00		1		7		-	1
15	30.7	0.0	0.8	21.5	0.0	1.4	15.7	1.0	1.6	120	1.1	1.8	D.A	1.1	21	7.4	1.2	2.5	6.A	1.4	2.8		4.	-			١.
30	40.9	0.0	8.0	28.6	0.9	1.5	20.0	1.0	1.4	18.3	1.0	1.0	12.0	1.1	21	10.1	1.2	2.5	8.0	1.3	29	8.2	1.4	3.3	1		1
25	51.1	0.8	0.0	35.0	0.9	1.1	26.1	1.0	1.4	20.3	T.O.	TE	15.0	1.1	21	12.7	1.2	2.5	10.2	1.3	2.0	8.2	1.4	3.6	6.5	1.5	1
30	61.3	0.9	0.8	42.0	0.0	1.1	31.4	1.0	1.4	24.4	1.0	1.8	19.2	1,1	21	15.2	12	2.5	12.3	1.3	2.0	10.0	1.3	3.4	8.1	1.5	13
35	71.5	0.0	0.0	50.1	0.9	1.1	36.6	1.0	1.4	28.3	1.0	1.0	22.A	1.1	2.1	10.0	12	2.5	14.4	1.2	2.9	11.7	13	34	9.0	1.4	13
40	51.8	0.0	0.0	57.2	0.9	1.1	41.8	1.0	1.5	32.4	1.0	1.8	25 A	1.1	21	20.8	1.2	2.5	16.5	1.2	2.0	13.5	1.3	3.4	11.1	1.4	1 3
45	02.0	0.9	0.8	84.4	0.9	1.1	47.0	1.0	1,5	36.4	1.0	1.5	25.5	1.1	21	23.1	12	2.5	18.8	1.2	2.9	15.2	1.3	3.4	12.0	1.4	1.3
50	102.2	0.0	0.6	71.5	0.9	1.1	52.2	1.0	1.5	40.5	1.0	1.0	32.0	1.1	21	25.7	12	2.5	30.9	1.2	2.9	17.0	1.3	3.4	14.0	14	13
56	1124	0.9	0.5	78.7	0.9	1.1	57.5	1.0	1.5	44.5	1.0	1.8	35.2	1,1	21	28.2	12	2.5	23.0	1.2	2.9	16.0	1.3	3.4	15.4	14	1 2
90	122.6	0.9	0.0	85.8	0.0	44	62.7	1.0	1.0	48,5	1.0	1.8	38.4	1.1	2.2	30.5	12	2.5	25.1	1.2	2.9	20.6	1.3	24	16.9	1.4	13
55	1328	0.9	0.8	93.0	0.9	1.4	67.9	1,0	1.5	52.8	1.0	1.5	41.5	1.1	22	33.4	12	2.6	27.2	1.2	2.0	22.3	1.3	3.4	18.3	1.4	T
70	143.1	0.9	0.8	100.1	0,9	1,1	73.1	1.0	1.5	56,8	1.0	1.8	44.7	14	22	35.0	1.2	25	29.2	12	2.9	24.0	1,3	3.4	20.0	1.4	1 2
75	153.3	0.0	0.8	107.3	0.0	1,1	70.3	1.0	1,5	80.7	1.0	1,0	47.9	1.1	2.2	38.5	1,2	2.5	31.3	1.2	2.9	25.7	1.3	3.4	21.4	1.4	10
60	163.5	0.8	0.0	114.4	0.9	1.5	63.6	1.0	1.5	04.7	1.0	1.0	51.1	1.1	22	41.0	12	2.5	33.4	1.2	2.9	27.4	1.3	3.4	22.8	14	12
86	173.7	QU	0.4	121.0	0.9	1.1	00.3	1.0	1.5	64.8	1.0	1.0	64.3	1.1	22	45.6	12	2.5	35.5	1.2	2.9	29,1	1.3	3.4	24.2	1.4	1 3
90	183.9	0.9	0.6	128.7	0.5	1.1	94.0	1,0	1,5	72.5	1.0	1,5	57.5	1.1	2.2	46.2	1.2	2.5	37.6	1.2	2.0	30.9	1.3	3.4	25.7	1.4	13
95	194.1	0.9	0.5	135.9	0.9	1.1	94.2	1.0	1.5	70.6	1.0	1.0	80.7	1.1	2.2	48.7	12	2.5	39.7	12	2.9	32.5	1.3	3.4	27.1	14	13
100	204.4	0.9	0.0	143.0	0.9	1.1	104.4	1.0	1,5	80.9	1.0	1.8	63.2	1.1	22	51.3	1.2	2.5	41.7	12	2.9	34.2	1.3	3.4	28.5	1.3	1 2
105	214.6	0.0	CA	150.2	8.0	1.1	109.7	1,0	1,6	84.9	1,0	1.5	67.1	1.1	2.2	53.9	1.2	2.5	43.6	1.2	2.9	35.9	1.3	34	29.9	1.3	1
10	224.8	0.0	4.0	157.A	0.9	1.1	114.0	1.0	1.5	59.0	1.0	1.0	70.3	14.	2.2	56.4	12	2.5	45.9	1.2	2.9	37.6	1.3	3.4	31.3	1.3	12
115	235.0	0.9	0.8	184.5	0.8	1.1	120.1	1.0	1.5	82.0	1.0	1,8	73.5	1.1	2.2	50.0	1.2	2.5	48.0	1.2	2.9	39.3	1.3	3.4	32.7	1.3	1
120	245.2	0.9		171,7	0.0	4.1	125.3	1.0	1.5	97,1	1.0	1.0	78.7	1.1	2.2	61.5	1.2	2.5	49.9	1.2	3,0	45.0	1.3	3.4	34.2	1.3	1.3
125	255.5	0.0	0.8	178.6	0.9	13	150.5	1,0	1.5	101,1	1.0	1.0	79.9	1.1	2.2	64.1	1.2	2.5	52.0	1.2	3.0	427	1.3	34	35.6	1.3	1
130	265.7	0.9	0.5	186.0	0.9	4.1	135.8	1.0	1.5	106.1	1.0	LB	63.0	3.1	2.2	66.7	1.2	2.5	54.1	12	3.0	44.4	1.3	3.4	37.0	1.3	1.2
135	275.9	0.0	0.6	193.1	0.9	1.1	141.0	1,0	1.5	100.2	1.0	1,5	56.2	1.1	2.2	69.2	1.2	2.6	58.1	12	3.0	46.1	1.3	3.4	38.4	1.3	12
140	286.1	0.9	0.8	200.3	0.9	1.1	145.2	1.0	1.5	113.2	1.0	1.5	89.4	1.1	2.2	71.8	12	2.5	58.2	1.2	3.0	47.8	1.3	3.4	30.9	1.3	1
145	296.3	0.9	0.5	207.4	0.9	1.1	151.4	1.0	1.5	117.3	1.0	1,5	82.5	1.1	7.2	74.A	1.2	2.5	60.3	1.2	3.0	48.6	1.3	34	41.3	13	1
150	300.5	0.9	0.8	214.6	0.0	1.1	156.7	1.0	1.5	121.5	1.0	1.0	95.5	1.1	2.2	76.9	1.2	2.6	62.4	1.2	3.0	51.3	1.3	3.4	42.7	13	1.3

Table DV-7 Parabolic Diversion Design Chart (Retardance "D" and "B," Grade 6.00%)

	1-20	5- 3-6	V	4-2.5		12.4	/1×4.0			11-35			/t==.0	-	٧	71-4.5			1=5.0	300		1-5.5			/1=6.0	۲.
7	DI	V2	T	D	V2	T	D	V2	1	D	V2	T	D	V2	Ŧ	D	V2	7	D	V2	T	D	V2	T	D	V
12.4	_	distance of	-	-		_	0.0	1.4	4.7	1.0	1.8	3.5	1.2	10						I To				1.00		
24.7	-	-		0.5	1.0	12.8	0.9	1.4	9.8	0.9	1.7	7.8	1,0	2.0	5.2	1.0	2.3	4.9	1.1	2.7	100		200	1	2	
37.1	0.7	0.8	26.4	0.5	1.1	19.2	0.8	1.4	15.0	0.0	1.7	11,8	6.9	2.0	9.5	1.0	2.4	-	1.1	-	-	-	-		-	3
49.A	0.7	0.8	35.1	0.8	1.1	25.6	0.8	1.4	19.0	0.0	1.7	16.0	0.9	20	12.9	1.0	2.4	10.4	1.0	-	8.5	1.1				-
81.2	0.7	0.0	43.9	0.6	1.1	32.0	8.0	1.4	24.9	0.0	1.7	128	0.0	2.0	16,1	1.0	2.4	13.1	1.0	2.5	10.0	NAME OF TAXABLE PARTY.	100			3
74.1	0.7	0.8	52.7	0.6	1.1	38.4	0.6	1.4	29.9	0.9	1,7	23,8	0.9	2.1	19.3	1.0	2.4				-	-		Annual Control	Service Annual Property lies	3
06.5	0.7	0.5	51.5	0,8	1.1	44.8	0.6	1.4	34.6	0.0	1.7	27.0	0.9	2.1	22.5	1,0	2.4	18.5	1.0	And the last	100	1.1	10000	-	-	3
95.9	Q.7	8.0	70.2	0.6	1.1	51.2	0.6	1.4	30.8	0.0	1.7	31.8	0.9	2.1		1000	And in case of	-	-	the same		1.1				3
11.2	0.7	0.6	79.0	0.8	1.1	57.0	0.6	14	44.8	0.9	The second second	35.7	0.9	2.1	29.0	1.0	24	25.6	1.0	-	And in column 2 is not a second	14	-	-	Name and	13
23.6	D.7	0.6	87.8	0.8	1.1	64.0	0.8	1.4	49.7	0.9	1.7	39.7	0.9	21	35.5	1.0	24			Printers and Print	-	-	Common or other death of the last of the l	-	-	13
36.0	0.7	0.6	90.6	0.0	1.1	70.4	0.5	1.4	54.7	0.9	1.7	43.6	0.9	_		1.00	St. Married	The second second		_		-	-			L
46.3	0.7	0.8	105.3	0.8	111	75.6	0.8	1.4	59.7	0.9	1.7	47.6	0.0		-	THE REAL PROPERTY.	Acres (Allerton)					THE PERSON NAMED IN			-	L
60.6	0.7	0.6	114.1	0.6	1.1	83.2	9.8	1.6	64.7	0.9	1,7	51,6	0.9	- Contractor	bendered by	(See) Section 1			-		Contraction of			and the second	Annual Property lies	
73.0	0.7	0.2	122.9	0.0	1.5	69.0	0.8	1.4	69.6	0.9	1.7	1	0.9	-		_	2 - 2	-	-			-			-	- 3
85.A	0.7	0.8	131.7	0.0	1.1	96.0	0.8	1.4	74.6	0.9	-	A. Carrier	-		-	Total Spins	-		43.00	_	Acres 1	-			-	13
97.7	0.7	0.8	140.4	0.6	1.1	102.3	0.6	14	79.5	0.0	_			200	-	-	_	_	1000000	The second			The second of	-	and the same	13
10.1	0.7	0.8	149.2	0.0	1.5	108.7	0,8	14	and the second	_	-	100	THE REAL PROPERTY.	-			Charles Andread	Annual Property		-		-	-	100000	100	13
22.4	0.7	0.8	158.0	0.8	1.1	115.1	0.8	1.4			ALC: UNKNOWN	-		-	THE RESERVE	-	-		-			-			A common	ti
24.6	0.7	0.8	Company of the Park of the Par	0.8	1.1		-	-	-		-			The same of	in the second	-			-	And in case of		46	- A. C. C. C.	Contract of the last	-	ti
H7.1	0.7	0.6	175.5	0.5	1.1	Section 2	and the last	-	_					Name of the Owner, where		D - C		-	Service year			-				13
59.5	0.7	0.0	The second second		-	The second second	and the same of		1 4 - 34 1		100	-				-	The second second		-		Annual Property lies	-		-	Interestina	nd-or
71.0				-	-	and the second		-	and the second	ALC TOWNSHIPS	or second		-		Annual Property and	_	_	-	and the same of	A PROPERTY.	10.10	-	Section 1981	The latest division in	and the same	1
84.2		Name and	PROPERTY. STATE OF THE PARTY OF		_	10.00		-	-		-	A CONTRACTOR OF THE PERSON NAMED IN	-	-		-	The Real Property lies	-	-			-	-	market and the	-	13
86.6	-	Section 1	and the second	-	-	- management	-	-	7.00	-	THE REAL PROPERTY.	Action to the last	411	_	THE PERSON NAMED IN	and the same of	and the same	-				-			Annual Property	
08.9			1.00	-	-		-	in the con-	La particular de la constante		-				-	-		_	-		_	_		The second	The same of	1
21.5	ALC: UNKNOWN	and the same of	Proposition of the Parket of t	-	-		-		-	And the last		4	10000	Automotion of			-	-	-		-	-		Charles St.	_	
-	-	-	the second	-	-	The second second	-	-			-	A Commission of the last	-		-	-	-	-	-		Total Street	-			-	
46.0		5.0	PERSONAL PROPERTY.		-	Automatic .	0.6	-	144.2	0.9	1.7	115.0	0.9	2.1	93.2	1.0	2.4	70.5	10	2.5	63.6	1.1	3.2	53.0	1.1	
	0.7	0.8	254.5	0.8	1.1	191.6	0,6	14	149.2	0.9	1.7	119.0	0.0	21	95.4	1.0	24	79.2	1.0	2.8	66.8	1.1	1.1	54.B	1.1	
70.7	0.7	6.0	253.3	0.8	1.1																					
されて、 中 日 日 日 日 日 日 日 日 日 日 日 日 日 日 日 日 日 日	57.1 69.4 69.4 69.4 60.5	20.7 0.7 57.1 0.7 59.4 0.7 59.4 0.7 51.8 0.7 74.1 0.7 76.5 0.7 10.5 0.7 11.2 0.7	22.4 0.7 0.8 24.7 0.7 0.4 57.1 0.7 0.8 59.4 0.7 0.8 59.8 0.7 0.8 59.8 0.7 0.8 56.5 0.7 0.8 56.5 0.7 0.8 56.5 0.7 0.8 56.5 0.7 0.8 56.5 0.7 0.8 56.6 0.7 0.8 56.0 0.7 0.8	22.4 0.7 0.8 8.7 24.7 0.7 0.8 17.8 25.1 0.7 0.8 38.1 26.4 0.7 0.8 38.1 27 0.8 38.1 28.8 0.7 0.8 43.9 26.1 0.7 0.8 52.7 26.5 0.7 0.8 52.7 26.5 0.7 0.8 52.7 26.5 0.7 0.8 70.2 21.2 0.7 0.8 70.2 21.2 0.7 0.8 70.2 21.3 0.7 0.8 105.3 20.6 0.7 0.8 105.3 20.6 0.7 0.8 114.1 27.0 0.8 105.3 20.6 0.7 0.8 131.7 27.7 0.7 0.8 140.4 21.1 0.7 0.8 158.8 22.4 0.7 0.8 158.8 22.4 0.7 0.8 158.8 22.4 0.7 0.8 158.8 22.4 0.7 0.8 158.8 22.4 0.7 0.8 158.8 24.0 0.7 0.8 158.8 25.5 0.7 0.8 1093.1 26.0 0.7 0.8 122.9 27.7 0.8 122.9 28.8 0.7 0.8 158.8 29.8 0.7 0.8 158.8 29.8 0.7 0.8 122.9 20.9 0.7 0.8 122.9 20.9 0.7 0.8 122.9 20.9 0.7 0.8 122.9 20.9 0.7 0.8 122.9	12.4 0.7 0.8 8.7 0.8 24.7 0.7 0.8 17.6 0.8 24.7 0.7 0.8 17.6 0.8 25.1 0.7 0.8 38.4 0.9 26.4 0.7 0.8 38.1 0.8 26.5 0.7 0.8 52.7 0.8 26.5 0.7 0.8 52.7 0.8 26.5 0.7 0.8 70.2 0.8 26.5 0.7 0.8 70.2 0.6 26.6 0.7 0.8 70.2 0.6 26.6 0.7 0.8 108.3 0.8 26.6 0.7 0.8 131.7 0.8 26.6 0.7 0.8 149.4 0.8 26.6 0.7 0.8 149.4 0.8 26.6 0.7 0.8 149.4 0.8 26.6 0.7 0.8 158.8 0.8 26.7 0.8 158.8 0.8 26.8 0.7 0.8 149.4 0.8 26.8 0.7 0.8 149.4 0.8 26.8 0.7 0.8 158.8 0.8 26.8 0.7 0.8 158.8 0.8 26.8 0.7 0.8 158.8 0.8 26.8 0.7 0.8 168.3 0.8 26.8 0.7 0.8 168.3 0.8 26.8 0.7 0.8 120.9 0.8 26.8 0.7 0.8 201.9 0.8 26.8 0.7 0.8 201.9 0.8 26.8 0.7 0.8 219.7 0.8 26.8 0.7 0.8 229.2 0.8	12.4 0.7 0.8 8.7 0.8 1.9 24.7 0.7 0.8 17.6 0.5 1.0 57.1 0.7 0.8 .28.4 0.5 1.1 19.4 0.7 0.8 38.1 0.8 1.1 19.8 0.7 0.8 38.1 0.8 1.1 26.5 0.7 0.8 52.7 0.4 1.1 26.5 0.7 0.8 51.5 0.0 1.1 28.9 0.7 0.8 70.2 0.6 1.1 22.6 0.7 0.8 70.2 0.6 1.1 23.6 0.7 0.8 70.2 0.6 1.1 23.6 0.7 0.8 70.2 0.6 1.1 23.6 0.7 0.8 70.2 0.6 1.1 23.6 0.7 0.8 70.2 0.8 1.1 24.0 0.7 0.8 105.3 0.8 1.1<	12.4 0.7 0.8 8.7 0.8 1.9 6.2 24.7 0.7 0.8 17.6 0.0 1.0 12.8 57.1 0.7 0.8 17.6 0.0 1.0 12.8 57.1 0.7 0.8 38.4 0.9 1.1 19.2 19.4 0.7 0.8 38.1 0.8 1.1 24.8 81.9 0.7 0.8 52.7 0.8 1.1 38.4 86.5 0.7 0.8 51.5 0.8 1.1 38.4 86.9 0.7 0.8 70.2 0.6 1.1 51.2 15.2 0.7 0.8 70.2 0.6 1.1 57.8 23.6 0.7 0.8 70.2 0.6 1.1 57.8 23.6 0.7 0.8 70.2 0.6 1.1 57.8 23.6 0.7 0.8 70.8 0.8 1.1 57.8 <	12.4 0.7 0.8 8.7 0.8 1.9 8.2 0.8 24.7 0.7 0.8 17.6 0.5 1.0 12.8 0.9 57.1 0.7 0.8 17.6 0.5 1.0 12.8 0.9 57.1 0.7 0.8 38.1 0.5 1.1 19.2 0.8 89.4 0.7 0.8 38.1 0.5 1.1 24.6 0.8 67.1 0.7 0.8 52.7 0.8 1.1 38.4 0.8 86.5 0.7 0.8 51.5 0.8 1.1 34.8 0.8 86.9 0.7 0.8 70.2 0.6 1.1 51.2 0.6 81.2 0.7 0.8 70.2 0.6 1.1 57.8 0.8 81.2 0.7 0.8 70.2 0.6 1.1 57.8 0.8 81.2 0.7 0.8 70.8 0.8 1.1 <	12.4 0.7 0.8 8.7 0.8 1.9 8.2 0.9 7.4 24.7 0.7 0.8 17.6 0.5 1.0 12.8 0.9 1.4 57.1 0.7 0.8 .28.4 0.6 1.1 19.2 0.8 1.4 19.4 0.7 0.8 38.1 0.8 1.1 19.2 0.8 1.4 19.8 0.7 0.8 38.9 0.8 1.1 23.6 0.8 1.4 26.5 0.7 0.8 52.7 0.4 1.7 38.4 0.6 1.4 26.5 0.7 0.8 51.5 0.8 1.1 44.8 0.6 1.4 26.5 0.7 0.8 70.2 0.4 1.1 57.9 0.6 1.4 27.0 0.8 70.2 0.4 1.1 57.9 0.6 1.4 28.9 0.7 0.8 77.9 0.8 1.1 57.9	12.4 0.7 0.8 8.7 0.8 1.9 8.2 0.8 1.4 4.7 24.7 0.7 0.8 17.6 0.5 1.0 12.8 0.9 1.4 8.8 57.1 0.7 0.8 38.4 0.9 1.1 19.2 0.8 1.4 15.0 19.4 0.7 0.8 38.1 0.8 1.1 19.2 0.8 1.4 19.0 31.8 0.7 0.8 38.1 0.8 1.1 38.4 0.8 1.4 24.9 34.1 0.7 0.8 52.7 0.8 1.1 38.4 0.8 1.4 24.9 36.5 0.7 0.8 51.5 0.8 1.1 38.4 0.8 1.4 24.8 38.9 0.7 0.8 70.2 0.6 1.1 51.2 0.5 1.4 38.3 15.2 0.7 0.8 70.2 0.6 1.1 57.0 0.5	12.4 0.7 0.8 8.7 0.8 1.9 8.2 0.9 1.4 4.7 1.0 24.7 0.7 0.8 17.6 0.5 1.0 12.8 0.9 1.4 6.8 0.5 57.1 0.7 0.8 17.6 0.5 1.0 12.8 0.9 1.4 6.8 0.5 57.1 0.7 0.8 38.1 0.8 1.1 19.2 0.8 1.4 15.0 0.9 99.8 0.7 0.8 38.1 0.8 1.1 22.8 0.8 1.4 19.0 0.9 96.5 0.7 0.8 52.7 0.8 1.1 38.4 0.8 1.4 24.9 0.9 96.5 0.7 0.8 51.5 0.8 1.1 38.4 0.8 1.4 24.8 0.9 98.9 0.7 0.8 70.2 0.6 1.1 57.0 0.6 1.4 44.8 0.9	12.4 0.7 0.8 8.7 0.8 1.9 6.2 0.8 1.4 4.7 1.0 1.2 24.7 0.7 0.8 17.6 0.8 1.0 12.8 0.9 1.4 9.8 0.5 1.7 57.1 0.7 0.8 38.4 0.6 1.1 19.2 0.8 1.4 15.0 0.9 1.7 99.4 0.7 0.8 38.1 0.8 1.1 19.2 0.8 1.4 15.0 0.9 1.7 91.8 0.7 0.8 38.1 0.8 1.1 38.4 0.8 1.4 24.9 0.9 1.7 96.5 0.7 0.8 55.7 0.8 1.1 38.4 0.8 1.4 24.9 0.9 1.7 96.5 0.7 0.8 70.2 0.8 1.1 54.8 0.8 1.4 24.9 0.9 1.7 98.9 0.7 0.8 70.2 0.8	12.4 0.7 0.8 8.7 0.8 1.9 8.2 0.9 1.4 4.7 1.0 1.8 3.5 24.7 0.7 0.8 17.6 0.5 1.0 12.8 0.9 1.4 9.6 0.5 1.7 7.8 57.1 0.7 0.8 126.4 0.8 1.1 19.2 0.8 1.4 15.0 0.9 1.7 7.8 19.4 0.7 0.8 38.1 0.8 1.1 19.2 0.8 1.4 15.0 0.9 1.7 11.8 19.8 0.7 0.8 38.1 0.8 1.1 38.4 0.8 1.4 19.9 0.9 1.7 18.9 19.5 0.7 0.8 51.5 0.0 1.1 38.4 0.8 1.4 24.9 0.9 1.7 22.8 85.9 0.7 0.8 70.2 0.6 1.1 57.8 0.6 1.4 24.8 0.9 1.7	12.4 0.7 0.8 8.7 0.8 1.9 8.2 0.9 1.4 4.7 1.0 1.8 3.5 1.2 24.7 0.7 0.8 17.6 0.0 1.0 12.8 0.9 1.4 9.8 0.8 1.7 7.8 1.0 57.1 0.7 0.8 38.4 0.8 1.1 19.2 0.8 1.4 15.0 0.9 1.7 11.8 0.8 19.4 0.7 0.8 38.1 0.8 1.1 19.2 0.8 1.4 19.0 0.9 1.7 11.8 0.9 19.8 0.7 0.8 35.7 0.8 1.1 38.4 0.8 1.4 24.9 0.9 1.7 23.8 0.9 26.5 0.7 0.8 51.5 0.8 1.1 44.8 0.8 1.4 34.8 0.9 1.7 23.8 0.9 27.7 0.8 70.2 0.8 1.1 57.0	12.4 0.7 0.8 8.7 0.8 1.9 8.2 0.9 1.4 4.7 1.0 1.8 2.5 1.2 1.9 24.7 0.7 0.8 17.6 0.5 1.0 12.8 0.9 1.4 6.8 0.8 1.7 7.8 1.0 2.0 57.1 0.7 0.8 38.4 0.6 1.1 19.2 0.8 1.4 15.0 0.9 1.7 11.8 0.9 2.0 19.4 0.7 0.8 38.1 0.8 1.1 19.2 0.8 1.4 19.0 0.9 1.7 11.8 0.9 2.0 19.8 0.7 0.8 35.7 0.6 1.1 38.4 0.8 1.4 24.9 0.9 1.7 23.8 0.9 2.1 85.9 0.7 0.8 70.2 0.4 1.1 36.4 0.6 1.4 34.8 0.9 1.7 23.8 0.9 2.1	12.4 0.7 0.8 8.7 0.8 1.9 8.2 0.9 1.4 4.7 1.0 1.8 3.5 1.2 1.8 24.7 0.7 0.8 17.6 0.5 1.0 12.8 0.9 1.4 6.8 0.5 1.7 7.8 1.0 2.0 5.2 57.1 0.7 0.8 32.4 0.8 1.1 19.2 0.8 1.4 15.0 0.9 1.7 11.8 0.8 2.9 9.9 1.7 11.8 0.8 2.9 9.9 1.7 18.0 0.9 2.0 15.1 31.8 0.7 0.8 52.7 0.8 1.1 38.4 0.8 1.4 24.9 0.9 1.7 23.8 0.9 2.1 19.3 85.9 0.7 0.8 70.2 0.6 1.1 54.8 0.8 1.4 34.8 0.9 1.7 23.8 0.9 2.1 22.5 85.9 0.7	124 0.7 0.8 8.7 0.8 1.0 8.2 0.8 7.4 4.7 1.0 1.8 3.5 1.2 1.8 124 0.7 0.8 17.8 0.6 1.0 12.8 0.9 1.4 8.8 0.8 1.7 7.8 1.0 2.0 5.2 1.0 157.1 0.7 0.8 1.28 0.8 1.1 19.2 0.8 1.4 15.0 0.9 1.7 11.8 0.8 2.0 9.5 1.0 157.1 0.7 0.8 38.1 0.8 1.1 19.2 0.8 1.4 19.0 0.9 1.7 11.8 0.8 2.0 9.5 1.0 159.8 0.7 0.8 45.9 0.8 1.1 38.4 0.8 1.4 19.0 0.9 1.7 18.8 0.9 2.0 18.1 1.0 159.8 0.7 0.8 52.7 0.8 1.1 38.4 0.8 1.4 29.9 0.9 1.7 23.8 0.9 2.1 19.3 1.0 159.8 0.7 0.8 52.7 0.8 1.1 38.4 0.8 1.4 34.8 0.9 1.7 27.0 0.9 2.1 22.5 1.0 159.9 0.7 0.8 57.2 0.6 1.1 51.2 0.5 1.4 34.8 0.9 1.7 27.0 0.9 2.1 22.5 1.0 159.9 0.7 0.8 70.2 0.6 1.1 51.2 0.5 1.4 38.8 0.9 1.7 27.8 0.9 2.1 22.5 1.0 159.9 0.7 0.8 70.2 0.6 1.1 51.2 0.5 1.4 38.8 0.9 1.7 38.7 0.8 2.1 22.5 1.0 159.9 0.7 0.8 70.2 0.6 1.1 54.0 0.8 1.4 44.8 0.9 1.7 38.7 0.8 2.1 22.5 1.0 159.9 0.7 0.8 70.8 0.8 1.1 54.0 0.8 1.4 44.8 0.9 1.7 30.7 0.9 2.1 32.2 1.0 159.9 0.7 0.8 90.8 0.8 1.1 70.4 0.5 1.4 54.7 0.9 1.7 30.7 0.9 2.1 32.4 1.0 159.0 0.7 0.8 108.3 0.8 1.1 76.8 0.8 1.4 54.7 0.9 1.7 47.6 0.9 2.1 36.4 1.0 159.0 0.7 0.8 108.3 0.8 1.1 76.8 0.8 1.4 54.7 0.9 1.7 50.5 0.9 2.1 36.4 1.0 159.0 0.7 0.8 149.2 0.8 1.1 100.7 0.8 1.4 54.7 0.9 1.7 50.5 0.8 2.1 45.0 1.0 159.0 0.7 0.8 149.2 0.8 1.1 100.7 0.8 1.4 54.7 0.9 1.7 50.5 0.9 2.1 54.7 1.0 159.1 0.7 0.8 149.2 0.8 1.1 100.7 0.8 1.4 54.5 0.9 1.7 76.8 0.9 2.1 54.7 1.0 159.1 0.7 0.8 149.2 0.8 1.1 140.7 0.8 1.4 140.		12.4 0.7 0.8 8.7 0.8 1.9 6.2 0.9 1.4 4.7 1.9 1.8 3.5 1.2 1.8	1. 1. 1. 1. 1. 1. 1. 1.						12.4 0.7 0.8 6.7 0.8 1.0 6.2 0.9 1.4 6.8 0.8 1.7 7.8 1.0 2.0 5.2 1.0 2.4 4.8 1.1 2.7 2.7 0.2 1.2 3.1 5.0 1.3 1.7 7.8 1.0 2.0 9.5 1.0 2.4 7.7 1.1 2.7 0.2 1.2 3.1 5.0 1.3 1.7 7.8 1.0 2.0 9.5 1.0 2.4 7.7 1.1 2.7 0.2 1.2 3.1 5.0 1.3 1.0 1.3

Table DV-8 Parabolic Diversion Design Chart (Retardance "D" and "B," Grade 8.00%)

												Gree	QB et	O Pe	rcent												
Q #8	-)	/1-2.0	3		/1-2.5	,	1	/1×3.0		10	/1=3,5		1	V1-4.0		10	/1=4.5		1	/1=5.0		-	1=5.5		0	/1 -6. 0	
0		6	V2	T	0	1 45	T	D	V2	Y	D	VŽ	*	0	V2	Ť	Ò	V2	*	D	V2	T	D	V2	1	D	V2
	14.0	0.7	0.8	10.1	0.7	1.0	7.4	9,8	13	5.5	0.0	1.5	44	0.9	1.0	3.4	1.0	21									
10	28.0	0.7	0.6	20.1	0.7	1.0	15.0	8.0	1.3	11.3	0.0	1.7	1.1	4.8	2.0	7.4	0.0	2.5	8.0	0.8	2.8	4.0	1.0	3.0	3.6	1.2	2.3
15	41.9	0.7	0.8	30.1	0.7	1.0	22.4	0.8	1.3	17.0	0.8	1.7	13.9	0.8	2.0	11.4	0.9	2.3	9.2	0.0	2.7	7.5	1.0	3.0	6.3	1.0	3.4
20	55.9	0,7	0.8	40.1	0.7	1.0	29.9	0,8	1.3	72.6	0.8	1.7	10.5	0.8	2.0	15.1	0.0	2.3	12.5	0.5	2.7	10.2	1.0	3.1	0.5	10	3.5
25	69.9	0.7	0.8	50.1	0.7	1.0	37.3	0.8	1.3	28.2	0.6	1.7	23.1	0.6	2.0	10.8	0.9	2.5	15.6	0,9	2,7	13.0	0,9	3.1	10.6	1.0	3.6
30	93.9	0.7	0.8	60.1	0.7	1.0	44.8	0.6	1.3	33.9	0.8	1.7	27.7	0.5	2.0	22.6	O.B	2.3	16.0	9.0	2.7	15.9	0.9	3.1	13.0	1.0	3.5
35	97.9	0.7	9,8	70.1	0.7	1.0	52.3	0.6	1.3	39.5	0.8	1.7	32.2	0.0	2.0	26.3	0.6	2.3	21.7	0.9	2.7	10.2	0.0	3.1	18,5	1.0	3.5
40	111.8	0.7	0.6	50.2	0.7	1.0	\$9.7	D.8	1.3	45,1	0.8	1.7	36.0	0.8	2.0	30.1	0.9	23	24.6	0.9	2,7	20.6	0.9	3.1	17.5	1.0	3.5
	125.0	0.7	0.8	80.2	0.7	1.0	67.2	0.8	1.3	50.6	0.6	1.7	41.5	0.0	20	33.6	G.S	2.2	27.9	0.9	2.7	23.2	2.9	3.1	19.7	1.0	3.5
2	158.8	0.7	_	100.2	0.7	1.0	74.7	0.6	1.3	55.4	0.5	1.7	46.1	0.0	20	37.6	6.8	23	31.0	0.9	2.7	25.9	0.0	31	21.0	1.0	2.5
80	167.0	0.7	8.0	110.2	0.7	1.0	621	8.8	1.3	621	B.6	1.7	50.7	_	20	41.3	0.9	23	34.1	0.9	2.7	28.5	0.0	31	24.0	1,0	3,5
84	181.7	0.7	0.8	130.3	0.7	1.0	97.0	0.8		733	0.8	1.7	55.3		2.0	45.1	0.9	2,5	37,2	0.0	2.7	31,1	0.9	2.1	28.2	1.0	2.5
70	105.7	0.7	8.0	140.3	0.7	1.0	104.5	0.0	1.3	79.0	0.0	1.7	64.5	0.0	2.0	48.0	0.0	23	40.3	0.9	2.7	33.7	0.9	71	28.4	1.0	3.5
75	209.7	0.7	0.8	150.3	0.7	1.0	112.0	0.8	13	84.8	0.8	1.7	69.2	0.5	2.0	56.3	0.0	23	45.4	0.9	27	38.3	0.9	31	30.6	1,0	3.5
90	221.7	0.7	0.8	190.3	0.7	1.0	119.4	0.6	13	90.3	0.0	1.7	73.6	0.6	2.0	60.1	0.0	2.3	49.6	0.0	27	41.4	0.0	3.1	32.0	1.0	3.5
-	237.7	0.7		170.3	0.7	1.0	126.9	0.0	1.3	85.9	0.0	1.7	78.4	0.8	2.0	63.6	0.0	23	52.7	0.0	27	44.0	0.0	31	37.1	1.0	1.5
	251.6	0.7	0.0	100.3	0.7	1.0	134.4	6.0	13	101.8	0.0	1.7	83.0	0.5	2.0	67.6	0.9	2.3	55.6	0.9	27	46,6	08	3.1	39.3	1,0	3.5
-	285.6	0.7	0.6	190.4	0.7	1.0	141.8	0.6	1.3	107.2	0.8	1.7	67.6	0.0	20	71.3	0.5	23	55.8	0.9	27	49.2	0.9	31	41.5	1.0	15
00	279.5	0.7	0.4	200.4	0.7	1.0	140.3	6.0	1.3	112.8	0.8	1.7	92.2	0.8	20	76.1	0.9	2.3	62.0	0.0	2.7	51.6	0.8	31	43.7	1.0	1.5
95	293.5	0.7	0.8	210.4	0.7	1.0	158.8	0.8	1.3	118.5	9.8	1.7	56.8	0.8	20	78.9	0.9	23	68.1	0.9	27	54.4	0.9	31	45.9	1.0	3.5
io	307.6	0.7	8.0	220,4	0.7	1.0	194.2	0.8	1.3	124.1	0.8	1.7	101.4	0.8	2.0	62.6	0.9	23	64.2	0.8	2.7	57.0	0.0	3.1	48.0	1.0	2.5
	321.5	0.7	0.0	230.4	0.7	1.0	171.7	0,8	1,3	129.8	0.5	1.7	106.1	0.0	2.0	86.4	0.9	23	71.3	0.0	2.7	59.6	0.9	3.1	50.2	1.0	15
_	335.5	0.7	0.6	240.5	0.7	1.0	179.1	9.8	1.3	135.4	0.8	1.7	110.7	0.8	20	99.1	0.9	23	74.4	0.9	2.7	62.2	0.0	3.1	52.4	1,0	3.5
-	340.5	0,7	0.8		0.7	1.0	186.6	0.5	1.3	141.0	0.8	1.7	115.3	6.0	2.0	93.9	0.9	23	77.5	0.9	27	64.7	0.9	3.1	54.6	1.0	3.5
-	363.5	0.7	0.5	200.5	0.7	1.9	184.1	0.5	1.3	145.7	9.6	1.7	119.9	6,0	20	97.6	0.9	2.3	90.6	0.9	2.7	67.3	0.0	3.1	50.8	1.0	2.8
-	377.5	0.7	0.8	270.5	0.7	1.0	201.5	0.8	1.2	162.3	0.8	1.7	124.5	0.8	2.0	101.4	0.9	2.3	83.7	0.0	27	60.9	0.9	2.1	59.0	1,0	3.5
1	391.5	0.7	8,6	200.5	0.7	1.0	206.0	6.8	1.2	155.0	0.8	1.7	129.1	0.8	2.0	105.1	0.8	23	6.89	0.0	27	72.5	0.9	3.1	61,1	1.0	3.5
45	419.4	0.7	0.8	290.6	0.7	1.0	216.5	0.8	1.3	163.5	0.8	1.7	133.7	9.6	2.0	108.9	0.0	23	69.0	0.0	2.7	75.1	0.9	2.1	65.3	1.0	2.5
50		0.7	0.5	300.6	0.7	1.0	223.9	0.8	1.3	169.3	0.6	1.7	130.3	0.8	20	112.6	0.8	23	83.0	0.9	2.7	77.7	0.9	2.5	84.5	1.0	3.5

Table DV-9 Parabolic Diversion Design Chart (Retardance "D" and "B," Grade 10.00%)

		1-2.0		11.19	/1×2.5	11	1	n-3.0		· 1	103.5	06	-	1-4.0	1		14.5	5.7		7=5.0		V	1=0.5	1	. 1	71=6.0	6
CES		0	VZ	7	0	V2	7	D	V2	T	D	V2	7	D	VZ	7	DI	V2	*	D	V2	T	D	V2	T	D	V
5	15.3	0.6	0.5	11.1	0.7	1.0	8.1	0.7	1.3	8.3	0.7	1.0	4.0	0.0	1.0	4.0	0.B	2.2	3.1	4.0	24	-					
10	30.6	0.6	0.8	22.1	9.7	1.0	16.5	0.7	1.3	12.8	0.7	1.6	10.0	0.0	20	0.4	D.B	2.2	6.9	0.8	2.5	5.7	0.0	2.0	4.7	1.0	X.
15	45.9	0.6	0.8	33.2	0.7	1.0	34.7	0.7	1.3	19.2	0.7	*#	15.0	0.5	20	12.7	0.8	2.2	10.5	G.A	2.8	0.7	0.0	3.0	7.3	0.9	3.
20	61.2	0.6	8.0	44.2	0.7	1.0	32.0	0.7	1.8	25.6	0.7	1.6	20.0	0.0	2.0	17.0	6.0	2.2	14.1	0.8	2.6	11.8	0.9	3.0	9.6	0.9	. 3/
25	70.6	0.6	O.B	55.3	0.7	1.0	41.1	0.7	1.5	32.0	0.7	1.6	25.0	0.8	2.0	21.2	8.0	2.3	17.5	0.8	2.8	14.7	0.9	3.0	12.6	0.9	3.
30	91.8	9.6	0.8	00.3	0.7	10	49.3	0.7	1.3	38.3	0.7	1,6	29.9	0.8	2.0	25.4	0.8	2.2	21.1	0.8	2.6	17.7	0.8	3.0	15.0	0.9	3.
35	107.1	0.6	0.8	77.4	0.7	1.0	57.5	0.7	1.3	44.7	0.7	1.6	34.9	0.0	2.0	29.7	0.6	2.3	24.6	0.8	2.8	20.6	0,8	3.0	17.5	0.0	3.
40	122.4	0.6	0.8	88.4	0.7	1.0	65.7	0.7	1.5	51.1	0.7	1.6	30.6	0.8	2.0	33.9	0.5	2.3	20.1	3.0	2.6	23.5	0.6	3,0	20.0	CD	3.
45	137.8	0.0	0.6	09.5	0.7	1.0	73.9	0.7	1.3	57.6	0.7	1.6	44.9	0.0	2.0	38.0	0.8	23	31.8	0.8	2.6	20.5	0.0	3.0	22.5	0.9	3.
50	153.1	0.4	0.8	110.6	0.7	10	82.1	0.7	1.3	03.9	0.7	1.8	40.9	8.0	2.0	42.2	8.0	23	35.1	0.0	2.8	29.4	0.0	3.0	25.0	0.9	3
55	168.4	0.6	0.8	121.0	0.7	1.0	90,3	0.7	1.5	70.3	0.7	1.6	54.9	0.6	2.0	46.4	0.8	2.3	30.6	0.6	2.6	32.3	0.8	3.0	27.5	0.0	3
60	163.7	0.0	0.8	132.7	0.7	1.0	98.5	0.7	1.3	70.7	0.7	1,8	59.9	0.6	2.0	60.7	0.0	2.3	42.1	0.0	2.6	35.3	0.8	3.0	30,0	0.9	3.
05	199.D	0.6	0.8		0.7	1.0	106.7	0.7	1.3	83.1	0.7	1.5	64.8	0.8	20	54.9	0.6	23	45,6	0.6	2.5	38.2	0.8	3.0	32.5	0.9	3
70	214.3	0.5	0.8	154.6	0.7	1.0	115.0	0.7	1.3	80,4	0.7	1.6	05.6	0.6	20	59.1	8.0	2.3	49.1	6.0	2.5	41.2	0.5	3,0	35.0	0.0	3
75	229.6	0.5	0.0	165.8	0.7	10	123.2	0.7	1.3	95.8	0.7	1,0	74.5	0.8	20	63.3	0.0	2.3	52.5	0.0	2.5	44.1	0.0	3.0	37,4	0.9	3
80	244.9	0.5	0.8	176.9	0.7	1.0.	131.4	0.7	1.3	102.2	0.7	1.6	79.8	0.0	2.0	67.6	0.6	23	56.1	0.8	2.8	47.0	0.8	3.0	39.1	0.0	3
85	200.2	0.0	0.8	187.9	0,7	1.0	139.6	0.7	1.3	108.6	0.7	1.8	84.6	0.8	20	71.8	0.8	2.3	59.5	0.5	2.6	50.0	0.6	3.0	42.3	0.9	2
90	275.5	0.6	0.8	199.0	0.7	1.0	147.8	0.7	1.3	115.0	0.7	1.6	8.86	0.8	20	78.0	D.A	23	63.1	0.6	2.6	52.9	0.8	3.0	44.0	0.9	3
95	290.8	0,6	0,5	210.0	0.7	1.0	150.0	0.7	13	121.4	0.7	1.5	94.6	0.0	2.0	80.2	0.6	23	65.6	0.5	2.5	56,6	0.8	3.0	47.2	0.9	3
100	306.1	0.0	0.8	221.1	0.7	1.0	184.2	0.7	13	127.8	0.7	1.5	29.5	0.4	2.0	54,4	9.0	23	70.1	0.8	2.5	58.0	0.8	3.0	49.7	0.9	13
105	321.6	0.0	0.0	232.2	0,7	1.0	1724	0.7	13	134.2	0.7	1.0	104.7	0.8	2.0	48.7	0.0	23	73.6	0.8	2.8	81.7	0.8	3.0	52.2	0.9	3
110	336.7	0.6	0,8	243.2	0.7	1.0	180.6	0,7	1,3	140.5	0.7	1.0	109.7	0.8	2.0	92.9	0.6	23	77.1	0.6	2.6	54.7	0.8	3.0	54.7	0.9	3
116	352.0	0.6	0.8	254.3	0.7	1.0	185 8	0.7	1.3	148.9	0.7	1.6	114.7	0.0	2.0	97.1	0.8	2.3	80,6	0.8	2.6	67.6	0.5	2.0	57.2	0.9	-
120	367,3	0.6	0.6	266.3	0.7	1.0	197.1	0.7	1.3	153.3	0.7	1.6	119.7	0.8	2.0	101.3	0.8	2.3	84.1	8.0	2.0	70.5	0.5	3.0	59.7	0.9	-
125	362.6	0.6	0.0	278.4	0.7	1.0	205.3	0,7	1.3	100.7	0.7	1.0	124.7	0.6	2.0	105.5	0.5	2.5	67.6	O.B	2.6	73.5	0.5	3.0	62.2	0.9	3
130	397.9	0.6	0.0	287.A	0.7	1.0	213.5	0.7	1.3	166.1	0.7	1.6	129.7	0.6	2.0	109.0	0.8	2.3	91.1	0.8	2.6	78.4	0.8	3.0	84,7	0.0	-
135	413.2	0,6	0.8	298.5	0.7	1.0	221.7	0.7	1.3	172.5	0.7	1.6	134.7	0.6	2.0	114.0	0.8	2.3	94.6	0.8	2.0	79.3	0,8	3.0	67,2	0.9	-
140	428,6	0.5	0.5	300.5	0.7	1.0	229.9	0.7	13	178.9	0.7	1.6	139.7	0.0	2.0	118.2	0.6	2.3	98.1	0.5	2.6	82,3	0.8	3.0	96.6	0.0	13
145	443.9	0.0	0.0	320.6	0.7	10	238,1	0.7	13	185.3	0.7	1.6	144.6	0.6	20	122.A	0.8	2.3	101.7	D.9	2.6	65.2	0.5	3.0	721	1	-
150	458 Z	4.0	0.8	331.7	0.7	1.0	248.3	0.7	1.3	191.6	0.7	1.0	148.6	0.6	2.0	126.7	0.6	23	105.2	0,8	2.6	186.2	0.9	1.0	74,6	0.9	13

Table DV-10 Parabolic Diversion Design Chart (Retardance "D" and "C," Grade .50%)

Q	1	1=2.0	× -	1	/1=2.5		,	/1=3.0		1	/1=3.5		2000	/1=4.0	3		/1=4.5		1	/1=5.0			/1=5.5		-	V1=6.0	1
CFS	Ŧ	D	V2	Т	D	V2	T		T		D	V2	T	D	V2	T	D	V2	Ť	D	V2	T	D	V2	Ť	D	V2
5	-	-	VZ	-	D	42		_D_	V2	T _		VZ.		U	VZ	-		V2			VZ			V2	148		
10	-	-	-	100		-		-		-	V.	1757	10 VF 16	130 1	CHY.	Da T		-				12.00			-	5	
15	8.4	1.6	1.7	-			-			1	-			7	1	-1	100		E BARRE	1		2"		5.5		100	
20	11.7	1.5	1.7	7.1	2.0	2.2	-		1	-					100	U			-	3			-				1
25	14.9	1.5	1.7	9.7	1.8	2.2	-	7			-	-				-		1	1011	111							1
30	18.0	1.5	1.7	12.0	1.7	2.2					7"				100		,	/					Se 25				
35	21.0	1.5	1.7	14.2	1.7	2.2	9.3	2.1	2.7		700 11	-					1	-	-	2	500		The I				
40	24.4	1.5	1.7	16.3	1.7	2.2	10.9	2.0	2.7	7	-	-	V 2000				1			100	0.00	X =		1		-	
45	27.4	1.5	1.7	18.5	1.7	2.2	12.5	2.0	2.7	11	-	-	1000		no Ties				-		ert at	5	1				
50	30.5	1.5	1.7	20.6	1.7	2.2	14.1	1.9	2.7	8.7	2.6	3.3	100.0010		part of the		2	-	See Jacks	713	4	-		1000	1	0	T
55	33.5	1.5	1.7	22.7	1.7	2.2	15.7	1.9	2.7	10.4	2.4	3.3		327	7	7500		V. 1-	2012	2		-	8	19.6	- 1		
60	36.6	1.5	1.7	24.8	1.7	2.2	17.2	1.9	2.7	11.7	2.3	3.3	7-1	1	April mely a				A		-14	1000	,	1		1	1
65	39.6	1.5	1.7	27.3	1.7	2.2	18.8	1.9	2.7	12.9	2.3	3.3	-	-	230	- 64		2.5	e entre				· ·		40.0		
70	42.6	1.5	1.7	29.4	1.7	2.2	20.3	1.9	2.7	14.0	2.2	3.3	9.8	2.8	3.8	177	-	-	-			1	-		24		
75	45.7	1.5	1.7	31.4	1.7	2.2	21.8	1.9	2.7	15.2	2.2	3.3	11.3	2.7	3.8		-7	7 - 1	2	1.01.7549	V X -y (1)	kipi	100		19.3		
80	48.7	1.5	1.7	33.5	1.7	2.2	23.3	1.9	2.7	16.3	2.2	3.3	12.2	2.6	3.8				- (n *	0	2 4	any is t					
85	51.7	1.5	1.7	35.6	1.6	2.2	24.8	1.9	2.7	17.4	2.2	3.3	13.2	2.5	3.8	-			7 0		100	210,-				X-	10
90	54.8	1.5	1.7	37.7	1.6	2.2	26.3	1.9	2.7	18.5	2.2	3.3	14.2	2.5	3.8	20		P	2. 7	6.	1 1/10	175 5 12			1		
95	57.8	1.5	1.7	39.8	1.6	2.2	27.8	1.9	2.7	19.6	2.2	3.3	15.1	2.5	3.8		-	1900	MO.								
100	60.9	1.5	1.7	41.9	1.6	2.2	29.7	1.9	2.7	20.7	2.2	3.3	16.0	2.5	3.8	11.0	3.2	4.3		120	- LA	500		10.3			
105	63.9	1.5	1.7	44.0	1.6	2.2	31.2	1.9	2.7	21.8	2.2	3.3	16.9	2.5	3.8	12.3	3.0	4.3	a- 1				Street L	1			
110	66.9	1.5	1.7	46.1	1.6	2.2	32.6	1.9	2.7	22.9	2.2	3.3	17.8	2.4	3.8	13.1	2.9	4.3	- 1	11			230			V.E.	
115	70.0	1.5	1.7	48.1	1.6	2.2	34.1	1.9	2.7	24.0	2.1	3.3	18.7	2.4	3.8	13.9	2.9	4.3	-					170		7	194
120	73.0	1.5	1.7	50.2	1.6	2.2	35.6	1.9	2.7	25.1	2.1	3.3	19.6	2.4	3.8	14.6	2.9	4.3		1 miles			190	1		10	
125	76.1	1.5	1.7	52.3	1.6	2.2	37.1	1.9	2.7	26.2	2.1	3.3	20.5	2.4	3.8	15.4	2.8	4.3	150						- 6	35	
130	79.1	1.5	1.7	54.4	1.6	2.2	38.5	1.9	2.7	27.3	2.1	3.3	21.3	2.4	3.8	16.1	2.8	4.3		- 1		- 1/2			- 96%:		
135	82.1	1.5	1.7	56.5	1.6	2.2	40.0	1.9	2.7	28.4	2.1	3.3	22.2	2.4	3.8	16.9	2.8	4.3			15					31.4	0-1
140	85.2	1.5	1.7	58.6	1.6	2.2	41.5	1.9	2.7	29.4	2.1	3.3	23.1	2.4	3.8	17.6	2.8	4.3	-700						- 2		
145	88.2	1.5	1.7	60.7	1.6	2.2	43.0	1.9	2.7	30.5	2.1	3.3	24.0	2.4	3.8	18.3	2.8	4.3	12.3	3.7	4.9						1
150	91.3	1.5	1.7	62.8	1.6	2.2	44.5	1.9	.2.7	31.6	2.1	3.3	24.8	2.4	3.8	19.0	2.7	4.3	13.1	3.5	4.9						

Table DV-11 Parabolic Diversion Design Chart (Retardance "D" and "C," Grade 1.00%)

Q	V	1=2.0		V	/1=2.5		\	/1=3.0		١	/1=3.5		27 V	1=4.0	A STATE OF	, v	1=4.5		V	1=5.0		V	1=5.5		٧	1=6.0	
CFS	T	D	V2	T	D	V2	T	D	V2	T SW	D	V2	To	D	V2	T	D	VŽ	T	D	V2 1	TI	D	V2	T	D	V
5			VZ.				133	-	-	1	-	- VZ						- '-		1111			7				1
10	8.2	1.2	1.6	5.2	1.4	2.0					724		10175			20		T-1	C-04			5	- h			1	
15	12.6	1.1	1.6	8.7	1.3	2.1	5.5	1.6	2.6	-						-	- 1			1			11				
20	17.1	1.1	1.6	11.8	1.2	2.1	8.2	1.4	2.6					1.34		-00							5		- 10		
25	21.4	1.1	1.6	14.9	1.2	2.1	10.5	1.4	2.6	7.3	1.6	3.1	200			7.				23	-	100				33	
30	25.7	1.1	1.6	18.0	1.2	2.1	12.8	1.4	2.6	9.1	1.6	3.2				3.	-	7.7	100	23	-	1.0	. 31	(80)			
35	29.9	1.1	1.6	21.2	1.2	2.1	15.0	1.3	2.6	10.9	1.5	3.1	7.8	1.8	3.7		3	-	-	15.4	23.6	333	13				11
40	34.2	1.1	1.6	24.3	1.2	2.1	17.3	1.3	2.6	12.6	1.5	3.1	9.2	1.7	3.7	-1			- 7		- 4	4.7	- 10	133			
45	38.5	1.1	1.6	27.3	1.2	2.1	19.5	1.3	2.6	14.3	1.5	3.1	10.6	1.7	3.7	7.2	2.2	4.3		15.	16.72	-		530			
50	42.7	1.1	1.6	30.3	1.2	2.1	21.9	1.3	2.6	16.0	1.5	3.2	11.9	1.7	3.7	8.8	2.0	4.3	700	***	-	10.00	11.3	-			
55	47.0	1.1	1.6	33.3	1.2	2.1	24.1	1.3	2.6	17.7	1.5	3.2	13.3	1.7	3.7	9.9	1.9	4.3	13	2.4	75.7	7.70	7	10.00			1
60	51.3	1.1	1.6	36.3	1.2	2.1	26.3	1.3	2.6	19.3	1.5	3.2	14.6	1.7	3.7	11.0	1.9	4.3		-	-	70.5	22.5	26			
65	2.00	1.1	1.6	39.4	1.2	2.1	28.5	1.3	2.6	21.0	1.5	3.2	15.9	1.6	3.7	12.1	1.9	4.3	8.0	2.5	4.9					- [
70	55.5 59.8	1.1	1.6	42.4	1.2	2.1	30.7	1.3	2.6	22.7	1.5	3.2	17.1	1.6	3.7	13.2	1.9	4.3	9.5	2.3	4.8	-					
-	64.1	_	1.6	45.4	1.2	2.1	32.9	1.3	2.6	24.6	1.5	3.1	18.5	1.6	3.7	14.2	1.8	4.3	10.4	2.2	4.9				- 30	-	
75	68.3	1.1	1.6	48.4	1.2	2.1	35.0	1.3	2.6	26.2	1.5	3.1	19.8	1.6	3.7	15.2	1.8	4.3	11.3	2.2	4.9						
80	72.6	1.1	1.6	51.5	1.2	2.1	37.2	1.3	2.6	27.9	1.5	3.1	21.0	1.6	3.7	16.3	1.8	4.3	12.1	2.2	4.9	8.8	2.7	5.4			
85	76.9	1.1	1.6	54.5	1.2	2.1	39.4	1.3	2.6	29.5	1.5	3.1	22.3	1.6	3.7	17.3	1.8	4.3	13.0	2.1	4.9	9.8	2.6	5.4			
90	81.1	_	1.6	57.5	1.2	2.1	41.6	1.3	2.6	31.1	1.5	3.1	23.6	1.6	3.7	18.3	1.8	4.3	13.8	2.1	4.9	10.9	2.5	5.3	***		1
95		1.1	1.6	60.5	1.2	2.1	43.8	1.3	2.6	32.7	1.5	3.1	24.9	1.6	3.7	19.3	1.8	4.3	14.6	2.1	4.9	11.6	2.4	5.4		-1	1
100	85.4	1.1	1.6	63.6	1.2	2.1	46.0	1.3	2.6	34.4	1.5	3.1	26.5	1.6	3.7	20.3	1.8	4.3	15.4	2.1	4.9	12.4	2.4	5.4	9.7	2.8	1
105	89.7		1.6	66.6	1.2	2.1	48.2	1.3	2.6	36.0	1.5	3.1	27.7	1.6	3.7	21.3	1.8	4.3	16.2	2.1	4.9	13.1	2.4	5.4	10.8	2.6	1
110	94.0	1.1	1.6	69.6	1.2	2.1	50.4	1.3	2.6	37.6	1.5	3.1	29.0	1.6	3.7	22.3	1.8	4.3	17.0	2.1	4.9	13.8	2.3	5.4	11.5	2.6	1
115	98.2	1.1	1.6	72.6	1.2	2.1	52.5	1.3	2.6	39.3	1.5	3.1	30.2	1.6	3.7	23.3	1.8	4.3	17.9	2.1	4.9	14.5	2.3	5.4	12.2	2.6	1
120	102.5	1.1	-	75.7	1.2	2.1	54.7	1.3	2.6	40.9	1.5	3.1	31.5	1.6	3.7	24.3	1.8	4.3	18.7	2.1	4.9	15.2	2.3	5.4	12.8	2.5	1
125	106.8	1.1	1.6	78.7	1.2	2.1	56.9	1.3	2.6	42.5	1.5	3.1	32.7	1.6	3.7	25.3	1.8	4.3	19.4	2.1	4.9	15.9	2.3	5.4	13.4	2.5	
130	111.0	-	_	81.7	1.2	2.1	59.1	1.3	2.6	44.2	1.5	3.1	34.0	1.6	3.7	26.3	1.8	4.3	20.2	2.0	4.9	16.6	2.3	5.4	14.1	2.5	
135	115.3	1.1	1.6		1.2	2.1	61.3	1.3	2.6	45.8	1.5	3.1	35.2	1.6	3.7	27.3	1.8	4.3	21.0	2.0	4.9	17.2	2.3	5.4	14.7	2.5	1
140	119.6	1.1	1.6	84.7					2.6	47.5	1.5		36.5	1.6	3.7	28.7	1.8	4.3	21.8	2.0	4.9	17.9	2.3	5.4	15.3	2.5	1
145	123.8	1.1	1.6	87.8	1.2	2.1	63.5	1.3	2.6	49.1	1.5	3.1	37.8		3.7	29.7	1.8	4.3	22.6	2.0	4.9	18.6	2.3	5.4	15.9	2.4	1
150	128.1	1.1	1.6	90.8	1.2	2.1	65.7	1.3	2.0	49.1	1.5	3.1	37.0	1.0	3.1	23.1	1.0	4.5	22.0	2.0	4.5	10.0		0.0	10.0		1

Table DV-12 Parabolic Diversion Design Chart (Retardance "D" and "C," Grade 2.00%)

Q CFS	١	/1=2.0		1	/1=2.5		٧	1=3.0			/1=3.5		٧	1=4.0	-	V	1=4.5		~	1=5.0		V	1=5.5	3.77	V	1=6.0	0
0.0	Ť	D	TV2	T	D	V2	T	D	V2	T	D	V2	T	D	V2	T	D	V2	T	D	V2	T	D	V2	T	D	V2
5	5.9	0.9	1.5																						-		
10	12.4	0.8	1.5	8.1	0.9	2.0	5.9	1.0	2.5			7.16	12.77	/ Fig.		A	-			0-10-1	364	a Division	150			100	
15	18.5	0.8	1.5	12.3	0.9	2.0	9.3	1.0	2.5	6.8	1.1	3.0	4.7	1.4	3.5		1								(m		
20	24.7	0.8	1.5	16.7	0.9	2.0	12.5	1.0	2.5	9.4	1.1	3.0	7.0	1.2	3.6	4.7	1.5	4.1					-41-		K 1		
25	30.8	0.8	1.5	20.8	0.9	2.0	15.9	1.0	2.4	11.8	1.1	3.0	9.0	1.2	3.5	6.8	1.3	4.1		10.00	100	-(.5	2.8	1.0		7.15	1
30	37.0	0.8	1.5	25.0	0.9	2.0	19.0	1.0	2.5	14.3	1.1	3.0	11.0	1.2	3.5	8.5	1.3	4.1	6.4	1.5	4.7	0.0				9	1 2
35	43.2	0.8	1.5	29.1	0.9	2.0	22.2	1.0	2.5	16.9	1.0	3.0	12.9	1.1	3.5	10.1	1.3	4.1	7.8	1.4	4.7			7°4		100	6.3
40	49.3	0.8	1.5	33.3	0.9	2.0	25.3	1.0	2.5	19.3	1.0	3.0	14.8	1.1	3.5	11.6	1.3	4.1	9.1	1.4	4.7	7.1	1.6	5.2		-37	11
45	55.5	0.8	1.5	37.4	0.9	2.0	28.5	1.0	2.5	21.7	1.0	3.0	16.7	1.1	3.5	13.1	1.3	4.1	10.4	1.4	4.7	8.2	1.6	5.2			
50	61.7	0.8	1.5	41.6	0.9	2.0	31.7	1.0	2.5	24.1	1.0	3.0	18.8	1.1	3.5	14.7	1.2	4.1	11.7	1.4	4.7	9.3	1.5	5.3	7.1	1.8	5.8
55	67.8	0.8	1.5	45.7	0.9	2.0	34.8	1.0	2.5	26.5	1.0	3.0	20.7	1.1	3.5	16.2	1.2	4.1	12.9	1.4	4.7	10.4	1.5	5.3	8.2	1.7	5.8
60	74.0	0.8	1.5	49.9	0.9	2.0	38.0	1.0	2.5	28.9	1.0	3.0	22.6	1.1	3.5	17.7	1.2	4.1	14.1	1.4	4.7	11.4	1.5	5.3	9.2	1.7	5.8
65	80.2	0.8	1.5	54.0	0.9	2.0	41.1	1.0	2.5	31.4	1.0	3.0	24.5	1.1	3.5	19.5	1.2	4.1	15.4	1.3	4.7	12.4	1.5	5.3	10.1	1.7	5.8
70	86.3	0.8	1.5	58.2	0.9	2.0	44.3	1.0	2.5	33.8	1.0	3.0	26.3	1.1	3.5	21.0	1.2	4.1	16.6	1.3	4.7	13.5	1.5	5.3	11.0	1.6	5.8
75	92.5	0.8	1.5	62.3	0.9	2.0	47.5	1.0	2.5	36.2	1.0	3.0	28.2	1.1	3.5	22.4	1.2	4.1	17.8	1.3	4.7	14.5	1.5	5.3	11.8	1.6	5.8
80	98.7	0.8	1.5	66.5	0.9	2.0	50.6	1.0	2.5	38.6	1.0	3.0	30.1	1.1	3.5	23.9	1.2	4.1	19.0	1.3	4.7	15.5	1.5	5.3	12.7	1.6	5.8
85	104.8	0.8	1.5	70.6	0.9	2.0	53.8	1.0	2.5	41.0	1.0	3.0	32.0	1.1	3.5	25.4	1.2	4.1	20.3	1.3	4.7	16.5	1.5	5.3	13.6	1.6	5.8
90	111.0	0.8	1.5	74.8	0.9	2.0	57.0	1.0	2.5	43.4	1.0	3.0	33.8	1.1	3.5	26.9	1.2	4.1	21.8	1.3	4.6	17.5	1.5	5.3	14.4	1.6	5.8
95	117.2	0.8	1.5	78.9	0.9	2.0	60.1	1.0	2.5	45.8	1.0	3.0	35.7	1.1	3.5	28.4	1.2	4.1	23.0	1.3	4.6	18.6	1.5	5.3	15.3	1.6	5.8
100	123.3	8.0	1.5	83.1	0.9	2.0	63.3	1.0	2.5	48.2	1.0	3.0	37.6	1.1	3.5	29.9	1.2	4.1	24.2	1.3	4.6	19.6	1.5	5.3	16.2	1.6	5.8
105	129.5	0.8	1.5	87.3	0.9	2.0	66.4	1.0	2.5	50.6	1.0	3.0	39.5	1.1	3.5	31.4	1.2	4.1	25.4	1.3	4.6	20.6	1.5	5.3	17.0	1.6	5.8
110	135.7	0.8	1.5	91.4	0.9	2.0	69.6	1.0	2.5	53.0	1.0	3.0	41.3	1.1	3.5	32.9	1.2	4.1	26.6	1.3	4.7	21.6	1.4	5.3	17.9	1.6	5.8
115	141.8	0.8	1.5	95.6	0.9	2.0	72.8	1.0	2.5	55.4	1.0	3.0	43.2	1.1	3.5	34.4	1.2	4.1	27.9	1.3	4.7	22.6	1.4	5.3	18.7	1.6	5.8
120	148.0	0.8	1.5	99.7	0.9	2.0	75.9	1.0	2.5	57.9	1.0	3.0	45.1	1.1	3.5	35.9	1.2	4.1	29.1	1.3	4.7	23.9	1.4	5.2	19.5	1.6	5.8
125	154.1	0.8	1.5	103.9	0.9	2.0	79.1	1.0	2.5	60.3	1.0	3.0	47.0	1.1	3.5	37.4	1.2	4.1	30.3	1.3	4.7	24.8	1.4	5.2	20.4	1.6	5.8
130	160.3	0.8	1.5	108.0	0.9	2.0	82.3	1.0	2.5	62.7	1.0	3.0	48.8	1.1	3.5	38.9	1.2		31.5	1.3	4.7	25.8	1.4	5.3	21.2	1.6	5.8
135	166.5	8.0	1.5	112.2	0.9	2.0	85.4	1.0	2.5	65.1	1.0	3.0	50.7	1.1	3.5	40.3	1.2	4.1	32.7	1.3	4.7	26.8	1.4	5.3	22.1	1.6	5.8
140	172.6	0.8	1.5	116.3	0.9	2.0	88.6	1.0	2.5	67.5	1.0	3.0	52.6	1.1	3.5	41.8	1.2	4.1	33.9	1.3	4.7	27.8	1.4	5.3	22.9	1.6	5.8
145	178.8	0.8	1.5	120.5	0.9	2.0	91.8	1.0	2.5	69.9	1.0	3.0	54.5	1.1	3.5	43.3	1.2	4.1	35.1	1.3	4.7	28.8	1.4	5.3	23.7	1.6	5.8
150	185.0	0.8	1.5	124.6	0.9	2.0	94.9	1.0	2.5	72.3	1.0	3.0	56.4	1.1	3.5	44.8	1.2	4.1	36.3	1.3	4.7	29.8	1.4	5.3	24.6	1.6	5.8

Table DV-13 Parabolic Diversion Design Chart (Retardance "D" and "C," Grade 4.00%)

		1			V1	FOR	RETAI	RDAN	NCE "	D", T			(T), E e 4.00			, AND) V2	FOR	RETA	RDA	NCE '	'C"		_ :			
Q	V1=2.0			V1=2.5			V	/1=3.0	70	\	/1=3.5		V	1=4.0		,	/1=4.5		, V1=5.0			1	/1=5.5	7.	١	/1=6.0	
GFS	T	D	V2	T	D	V2	T	D	V2	T	D	V2	T	D	V2	T	D	V2	7	D	V2	T	D	V2	T	D	V2
5	8.5	0.6	1.4	5.9	0.7	1.8	4.1	0.8	2.3						T 50	6-1-1	7 10										
10	17.2	0.6	1.4	12.1	0.7	1.8	8.8	0.7	2.3	6.7	0.8	2.8	5.2	0.9	3.3	3.8	1.0	3.9									1
15	25.8	0.6	1.4	18.1	0.7	1.8	13.4	0.7	2.3	10.3	0.8	2.8	8.1	0.8	3.4	6.4	0.9	3.9	4.9	1.0	4.5	117					
20	34.4	0.6	1.4	24.2	0.7	1.8	17.8	0.7	2.3	13.9	0.8	2.8	10.9	0.8	3.4	8.7	0.9	3.9	6.9	1.0	4.5	5.5	1.1	5.0	40.2		
25	43.0	0.6	1.4	30.2	0.7	1.9	22.3	0.7	2.3	17.4	0.8	2.8	13.8	0.8	3.3	10.9	0.9	3.9	8.8	1.0	4.5	7.1	1.0	5.1	5.7	1.2	5.6
30	51.6	0.6	1.4	36.3	0.7	1.9	26.7	0.7	2.3	20.8	0.8	2.8	16.5		3.3	13.2	0.9	3.9	10.7	0.9	4.5	8.7	1.0	5.1	7.1	1.1	5,6
35	60.2	0.6	1.4	42.3	0.7	1.9	31.1	0.7	2.3	24.3	0.8	2.8	19.3	0.8	3.4	15.6	0.9	3.9	12.5	0.9	4.5	10.3	1.0	5.0	8.4	1.1	5.6
40	68.8	0.6	1.4	48.3	0.7	1.9	35.6	0.7	2.3	27.8	0.8	2.8	22.0	0.8	3.4	17.8	0.9	3.9	14.4	0.9	4.5	11.8	1.0	5.0	9.8	1,1	5.7
45	77.4	0.6	1.4	54.4	0.7	1.9	40.0	0.7	2.4	31.2	0.8	2.8	24.8	0.8	3.4	20.0	0.9	3.9	16.4	0.9	4.4	13.3	1.0	5.0	11.1	1.1	5.7
50	86.0	0.6	1.4	60.4	0.7	1.9	44.5	0.7	-2.4	34.7	0.8	2.8	27.5	0.8	3.4	22.2	0.9	3.9	18.2	0.9	4.4	14.9	1.0	5.0	12.3	1.1	5.7
55	94.6	0.6	1.4	66.5	0.7	1.9	48.9	0.7	2.4	38.2	0.8	2.8	30.3	0.8	3.4	24.4	0.9	3.9	20.0	0.9	4.4	16.6	1.0	5.0	13.6	1.1	5.7
60	103.2	0.6	1.4	72.5	0.7	1.9	53.4	0.7	2.4	41.7	0.8	2.8	33.0	0.8	3.4	26.6	0.9	3.9	21.8	0.9	4.5	18.1	1.0	5.0	14.9	1.1	5.7
65	111.8	0.6	1.4	78.5	0.7	1.9	57.8	0.7	2.4	45.1	0.8	2.8	35.8	0.8	3.4	28.9	0.9	3.9	23.6	0.9	4.5	19.6	1.0	5.0	16.2	1.1	5.7
70	120.4	0.6	1.4	84.6	0.7	1.9	62.3	0.7	2.4	48.6	0.8	2.8	38.6	0.8	3.4	31.1	0.9	3.9	25.4	0.9	4.5	21.1	1.0	5.0	17.7	1.1	5.6
75	129.0	0.6	1.4	90.6	0.7	1.9	66.7	0.7	2.4	52.1	0.8	2.8	41.3	0.8	3.4	33.3	0.9	3.9	27.2	0.9	4.5	22.6	1.0	5.0	19.0	1,1	5.6
80	137.6	0.6	1.4	96.7	0.7	1.9	71.2	0.7	2.4	55.5	0.8	2.8	44.1	0.8	3.4	35.5	0.9	3.9	29.1	0.9	4.5	24.1	1.0	5.0	20.2	1.1	5.6
85	146.2	0.6	1.4	102.7	0.7	1.9	75.6	0.7	2.4	59.0	0.8	2.8	46.8	0.8	3.4	37.7	0.9	3.9	30.9	0.9	4.5	25.6	1.0	5.0	21.5	1.1	5.6
90	154.8	0.6	1.4	108.7	0.7	1.9	80.0	0.7	2.4	62.5	0.8	2.8	49.6	0.8	3.4	39.9	0.9	3.9	32.7	0.9	4.5	27.1	1.0	5.0	22.8	1.1	5.6
95	163.4	0.6	1.4	114.8	0.7	1.9	84.5	0.7	2.4	65.9	0.8	2.8	52.3	0.8	3.4	42.2	0.9	3.9	34.5	0.9	4.5	28.6	1.0	5.0	24.0	1.1	5.6
100	172.0	0.6	1.4	120.8	0.7	1.9	88.9	0.7	2.4	69.4	0.8	2.8	55.1	0.8	3.4	44.4	0.9	3.9	36.3	0.9	4.5	30.1	1.0	5.0	25.3	1.1	5.6
105	180.6	0.6	1.4	126.9	0.7	1.9	93.4	0.7	2.4	72.9	0.8	2.8	57.8	0.8	3.4	46.6	0.9	3.9	38.1	0.9	4.5	31.6	1.0	5.0	26.5	1.1	5.6
110	189.2	0.6	1.4	132.9	0.7	1.9	97.8	0.7	2.4	76.3	0.8	2.8	60.6	0.8	3.4	48.8	0.9	3.9	39.9	0.9	4.5	33.1	1.0	'5.0	27.8	1.1	5.6
115	197.8	0.6	1.4	138.9	0.7	1.9	102.3	0.7	2.4	79.8	0.8	2.8	63.3	0.8	3.4	51.0	0.9	3.9	41.7	0.9	4.5	34.6	1.0	5.0	29.0	1.1	5.6
120	206.4	0.6	1.4	145.0	0.7	1.9	106.7	0.7	2.4	83.3	0.8	2.8	66.1	0.8	3.4	53.3	0.9	3.9	43.6	0.9	4.5	36.1	1.0	5.0	30.2	1.1	5.7
125	215.0	0.6	1.4	151.0	0.7	1.9	111.2	0.7	2.4	86.8	0.8	2.8	68.8	0.8	3.4	55.5	0.9	3.9	45.4	0.9	4.5	37.6	1.0	5.0	31.5	1.1	5.7
130	223.7	0.6	1.4	157.1	0.7	1.9	115.6	0.7	2.4	90.2	0.8	2.8	71.6	0.8	3.4	57.7	0.9	3.9	47.2	0.9	4.5	39.1	1.0	5.0	32.7	1.1	5.7
135	232.3	0.6	1.4	163.1	0.7	1.9	120.1	0.7	2.4	93.7	0.8	2.8	74.3	0.8	3.4	59.9	0.9	3.9	49.0	0.9	4.5	40.6	1.0	5.0	34.0	1.1	5.7
140	240.9	0.6	1.4	169.1	0.7	1.9	124.5	0.7	2.4	97.2	0.8	2.8	77.1	0.8	3.4	62.1	0.9	3.9	50.8	0.9	4.5	42.1	1.0	5.0	35.2	1.1	5.7
145	249.5	0.6	1.4	175.2	0.7	1.9	129.0	0.7	2.4	100.6	0.8	2.8	79.8	0.8	3.4	64.3	0.9	3.9	52.6	0.9	4,5	43.6	1.0	5.0	36.5	1.1	5.7
150	258.1	0.6	1.4	181.2	0.7	1.9	133.4	0.7	2.4	104.1	0.8	2.8	82.6	0.8	3.4	66.6	0.9	3.9	54.4	0.9	4.5	45.1	1.0	5.0	37.8	1.1	5.7

RETARDANCE "D" AND "C"

Table DV-14 Parabolic Diversion Design Chart (Retardance "D" and "C," Grade 6.00%)

												Grac	ie 6.00	Per	cent												
Q	V1=2.0			V1=2.5			V1=3.0			٧	1=3.5	70	١.	/1=4.0		V1=4.5			V1=5.0			V1=5.5			V1=6.0		
	T	D	V2	T	D	V2	T	D	V2	100	. D	V2	T	D	V2	J	D	V2	T	D	V2	T	D	V2	T	D	V2
5	10.6	0.5	1.3	7.3	0.6	1.8	5.3	0.6	2.3	4.0	0.7	2.8	2.9	8.0	3.2												
10	21.1	0.5	1.3	14.7	0.6	1.8	10.9	0.6	2.3	8.4	0.7	2.8	6.6	0.7	3.2	5.3	8.0	3.8	4.2	8.0	4.3	4		1000			
15	31.6	0.5	1.3	22.1	0.6	1.8	16.3	0.6	2.3	12.7	0.6	2.7	10.1	0.7	3.3	8.2	0.7	3.8	6.6	0.8	4.3	5.4	0.9	4.9	4.3	1.0	5.5
20	42.1	0.5	1.3	29.5	0.6	1.8	21.7	0.6	2.3	17.0	0.6	2.7	13.6	0.7	3.2	11.1	0.7	3.7	9.0	0.8	4.3	7.4	0.8	4.9	6.1	0.9	5.5
25	52.7	0.5	1.3	36.8	0.6	1.8	27.1	0.6	2.3	21.2	0.6	2.8	17.0	0.7	3.2	13.9	0.7	3.8	11.3	0.8	4.3	9.3	8.0	4.9	7.8	0.9	5.5
30	63.2	0.5	1.3	44.2	0.6	1.8	. 32.5	0.6	2.3	25.4	0.6	2.8	20.4	0.7	3.2	16.6	0.7	3.8	13.7	8.0	4.3	11.3	8.0	4.9	9.4	0.9	5.5
35	73.7	0.5	1.3	51.6	0.6	1.8	38.0	0.6	2.3	29.7	0.6	2.8	23.8	0.7	3.2	19.4	0.7	3.8	16.0	0.8	4.3	13.4	0.8	4.9	11.1	0.9	5.5
40	84.2	0.5	1.3	58.9	0.6	1.8	43.4	0.6	2.3	33.9	0.6	2.8	27.2	0.7	3.3	22.2	0.7	3.8	18.3	0.8	4.3	15.3	0.8	4.9	12.7	0.9	5.5
45	94.8	0.5	1.3	66.3	0.6	1.8	48.8	0.6	2.3	38.2	0.6	2.8	30.7	0.7	3.3	24.9	0.7	3.8	20.6	0.8	4.3	17.2	0.8	4.9	14.5	0.9	5.4
50	105.3	0.5	1.3	73.6	0.6	1.8	54.2	0.6	2.3	42.4	0.6	2.8	34.1	0.7	3.3	27.7	0.7	3.8	22.8	0.8	4.3	19.1	0.8	4.9	16.1	0.9	5.4
55	115.8	0.5	1.3	81.0	0.6	1.8	59.7	0.6	2.3	46.6	0.6	2.8	37.5	0.7	3.3	30.5	0.7	3.8	25.1	0.8	4.3	21.0	0.8	4.9	17.7	0.9	5.4
60	126.4	0.5	1.3	88.4	0.6	1.8	65.1	0.6	2.3	50.9	0.6	2.8	40.9	0.7	3.3	33.3	0.7	3.8	27.4	0.8	4.3	22.9	0.8	4.9	19.3	0.9	5.4
65	136.9	0.5	1.3	95.7	0.6	1.8	70.5	0.6	2.3	55.1	0.6	2.8	44.3	0.7	3.3	36.0	0.7	3.8	29.7	0.8	4.3	24.8	0.8	4.9	20.9	0.9	5.4
70	147.4	0.5	1.3	103.1	0.6	1.8	75.9	0.6	2.3	59.3	0.6	2.8	47.7	0.7	3.3	38.8	0.7	3.8	32.0	8.0	4.3	26.7	0.8	4.9	22.5	0.9	5.4
75	158.0	0.5	1.3	110.5	0.6	1.8	81.3	0.6	2.3	63.6	0.6	2.8	51.1	0.7	3.3	41.6	0.7	3.8	34.3	0.8	4.3	28.6	0.8	4.9	24.1	0.9	5.4
80	168.5	0.5	1.3	117.8	0.6	1.8	86.8	0.6	2.3	67.8	0.6	2.8	54.5	0.7	3.3	44.3	0.7	3.8	36.5	8.0	4.3	30.5	0.8	4.9	25.7	0.9	5.5
85	179.0	0.5	1.3	125.2	0.6	1.8	92.2	0.6	2.3	72.0	0.6	2.8	57.9	0.7	3.3	47.1	0.7	3.8	38.8	0.8	4.3	32.4	0.8	4.9	27.3	0.9	5.5
90	189.6	0.5	1.3	132.6	0.6	1.8	97.6	0.6	2.3	76.3	0.6	2.8	61.3	0.7	3.3	49.9	0.7	3.8	41.1	0.8	4.3	34.3	0.8	4.9	28.9	0.9	5.5
95	200.1	0.5	1.3	139.9	0.6	1.8	103.0	0.6	2.3	80.5	0.6	2.8	64.7	0.7	3.3	52.6	0.7	3.8	43.4	0.8	4.3	36.2	0.8	4.9	30.5	0.9	5.5
100	210.6	0.5	1.3	147.3	0.6	1.8	108.5	0.6	2.3	84.8	0.6	2.8	68.1	0.7	3.3	55.4	0.7	3.8	45.7	0.8	4.3	38.1	0.8	4.9	32.1	0.9	5.5
105	221.1	0.5	1.3	154.6	0.6	1.8	113.9	0.6	2.3	89.0	0.6	2.8	71.5	0.7	3.3	58.2	0.7	3.8	47.9	0.8	4.3	40.0	0.8	4.9	33.7	0.9	5.5
110	231.7	0.5	1.3	162.0	0.6	1.8	119.3	0.6	2.3	93.2	0.6	2.8	74.9	0.7	3.3	60.9	0.7	3.8	50.2	0.8	4.3	41.9	0.8	4.9	35.3	0.9	5.5
115	242.2	0.5	1.3	169.4	0.6	1.8	124.7	0.6	2.3	97.5	0.6	2.8	78.3	0.7	3.3	63.7	0.7	3.8	52.5	0.8	4.3	43.8	0.8	4.9	36.9	0.9	5,5
120	252.7	0.5	1.3	176.7	0.6	1.8	130.2	0.6	2.3	101.7	0.6	2.8	81.7	0.7	3.3	66.5	0.7	3.8	54.8	0.8	4.3	45.7	0.8	4.9	38.5	0.9	5.5
125	263.3	0.5	1.3	184.1	0.6	1.8	135.6	0.6	2.3	106.0	0.6	2.8	85.1	0.7	3.3	69.3	0.7	3.8	57.1	0.8	4.3	47.6	0.8	4.9	40.1	0.9	5.5
130	273.8	0.5	1.3	191.5	0.6	1.8	141.0	0.6	2.3	110.2	0.6	2.8	88.5	0.7	3.3	72.0	0.7	3.8	59.4	0.8	4.3	49.5	0.8	4.9	41.7	0.9	5.5
135	284.3	0.5	1.3	198.8	0.6	1.8	146.4	0.6	2.3	114.4	0.6	2.8	91.9	0.7	3.3	74.8	0.7	3.8	61.6	0.8	4.3	51.4	0.8	4.9	43.3	0.9	5.5
140	294.9	0.5	1.3	206.2	0.6	1.8	151.8	0.6	2.3	118.7	0.6	2.8	95.3	0.7	3.3	77.6	0.7	3.8	63.9	0.8	4.3	53.3	8.0	4.9	44.9	0.9	5.5
145	305.4	0.5	1.3	213.6	0.6	1.8	157.3	0.6	2.3	122.9	0.6	2.8	98.7	0.7	3.3	80.3	0.7	3.8	66.2	0.8	4.3	55.2	0.8	4.9	46.5	0.9	5.5
150	315.9	0.5	1.3	220.9	0.6	1.8	162.7	0.6	2.3	127.1	0.6	2.8	102.1	0.7	3.3	83.1	0.7	3.8	68.5	0.8	4.3	57.1	0.8	4.9	48.1	0.9	5.5

RETARDANCE "D" AND "C"

Table DV-15 Parabolic Diversion Design Chart (Retardance "D" and "C," Grade 8.00%)

													de 8.0	102		pi recine											
Q CFS	V1=2.0			V1=2.5			1	/1=3.0		1	/1=3.5		1	/1=4.0		,	/1=4.5			/1=5.0		•	/1=5.5		,	/1=6.0)
	T	D	V2	T	D	V2	Ŧ	D	V2	Ŧ	Ď	V2	Ť	D	V2	Ŧ	D	V2	Ŧ	D	V2	Ŧ	D	V2	Ŧ	D	V2
5	12.0	0.5	1.3	8.5	0.5	1.7	6.2	0.5	2.2	4.6	0.6	2.7	3.7	0.6	3.2	2.9	0.7	3.6									T
10	24.1	0.5	1.3	16.9	0.5	1.7	12.6	0.5	2.2	9.6	0.6	2.7	7.8	0.6	3.2	6.3	0.6	3.7	5.1	0.7	4.2	4.2	0.8	4.8	3.2	0.9	5.3
15	36.1	0.5	1.3	25.3	0.5	1.7	18.9	0.5	2.2	14.4	0.6	2.7	11.8	0.6	3.2	9.7	0.6	3.7	7.9	0.7	4.2	6.5	0.7	4.8	5.4	0.8	5.
20	48.1	0.5	1.3	33.8	0.5	1.7	25.2	0.5	2.2	19.2	0.6	2.7	15.8	0.6	3.2	12.9	0.6	3.7	10.7	0.7	4.2	8.8	0.7	4.8	7.4	0.8	5.
25	60.1	0.5	1.3	42.2	0.5	1.7	31.5	0.5	2.2	24.0	0.6	2.7	19.7	0.6	3.2	16.2	0.6	3.7	13.4	0.7	4.2	11.2	0.7	4.7	9.3	0.8	5.
30	72.1	0.5	1.3	50.6	0.5	1.7	37.8	0.5	2.2	28.8	0.6	2.7	23.6	0.6	3.2	19.4	0.6	3.7	16.1	0.7	4.2	13.5	0.7	4.8	11.3	0.7	5.3
35	84.1	0.5	1.3	59.1	0.5	1.7	44.1	0.5	2.2	33.6	0.6	2.7	27.6	0.6	3.2	22.6	0.6	3.7	18.7	0.7	4.2	15.7	0.7	4.8	13.3	0.7	5.3
40	96.2	0.5	1.3	67.5	0.5	1.7	50.4	0.5	2.2	38.4	0.6	2.7	31.5	0.6	3.2	25.8	0.6	3.7	21.4	0.7	4.2	17.9	0.7	4.8	15.2	0.7	5.3
45	108.2	0.5	1.3	76.0	0.5	1.7	56.7	0.5	2.2	43.2	0.6	2.7	35.4	0.6	3.2	29.0	0.6	3.7	24.1	0.7	4.2	20.2	0.7	4.8	17.1	0.7	5.3
50	120.2	0.5	1.3	84.4	0.5	1.7	63.0	0.5	2.2	48.0	0.6	2.7	39.4	0.6	3.2	32.3	0.6	3.7	26.8	0.7	4.2	22.4	0.7	4.8	19.0	0.7	5.
55	132.2	0.5	1.3	92.8	0.5	1.7	69.3	0.5	2.2	52.8	0.6	2.7	43.3	0.6	3.2	35.5	0.6	3.7	29.4	0.7	4.2	24.7	_0.7	4.8	20.9	0.7	5.
60	144.2	0.5	1.3	101.3	0.5	1.7	75.6	0.5	2.2	57.6	0.6	2.7	47.2	0.6	3.2	38.7	0.6	3.7	32.1	0.7	4.2	26.9	0.7	4.8	22.8	0.7	5.
65	156.3	0.5	1.3	109.7	0.5	1.7	81.8	0.5	2.2	62.4	0.6	2.7	51.2	0.6	3.2	41.9	0.6	3.7	34.8	0.7	4.2	29.1	0.7	4.8	24.7	0.7	5.
70	168.3	0.5	1.3	118.2	0.5	1.7	88.1	0.5	2.2	67.2	0.6	2.7	55.1	0.6	3.2	45.2	0.6	3.7	37.5	0.7	4.2	31.4	0.7	4.8	26.6	0.7	5.
75	180.3	0.5	1.3	126.6	0.5	1.7	94.4	0.5	2.2	72.0	0.6	2.7	59.0	0.6	3.2	48.4	0.6	3.7	40.1	_0.7_	4.2	33.6	0.7	4.8	28.5	0.7	5.
80	192.3	0.5	1.3	135.0	0.5	1.7	100.7	0.5	2.2	76.8	0.6	2.7	63.0	0.6	3.2	51.6	0.6	3.7	42.8	0.7	4.2	35.9	0.7	4.8	30.3	0.7	5.
85	204.3	0.5	1.3	143.5	0.5	1.7	107.0	0.5	2.2	81.6	0.6	2.7	66.9	0.6	3.2	_ 54.9	0.6	3.7	45.5	0.7	4.2	38.1_	0.7	4.8	32.2	0.7	5.3
90	216.4	0.5	1.3	151.9	0.5	1.7	113.3	0.5	2.2	86.4	0.6	2.7	70.8	0.6	3.2	58.1	0.6	3.7	48.1	0.7	4.2	40.3	0.7	4.8	34.1	0.7	5.3
95	228.4	0.5	1.3	160.3	0.5	1.7	119.6	0.5	2.2	91.2	0.6	2.7	74.8	0.6	3.2	61.3	0.6	3.7	50.8	0.7	4.2	42.6	_0.7	4.8	36.0	0.7	5.3
00	240.4	0.5	1.3	168.8	0.5	1.7	125.9	0.5	2.2	96.0	0.6	2.7	78.7	_ 0.6	3.2	64.5	0.6	3.7	53.5	_0.7	4.2	44.8	0.7	4.8	37.9	0.7	5.3
-	264.4	0.5	1.3	177.2	0.5	1.7	132.2	0.5	2.2	100.8	0.6	2.7	82.6	0.6	3.2	67.8	0.6	3.7	56.2	0.7	4.2	47.1	0.7	4.8	39.8	0.7	5.3
10	276.5	0.5	1.3	185.7	0.5	1.7	138.5	0.5	2.2	110.4	0.6	2.7	86.6	_ 0.6	3.2	71.0	0.6	3.7	58.8	0.7	4.2	49.3	0.7	4.8	41.7	0.7	5.3
	288.5	0.5	1.3	202.5	0.5	1.7	144.8	0.5	2.2	115.2	0.6	2.7	90.5	0.6	3.2	74.2	0.6	3.7	61.5	0.7	4.2	51.5	0.7	4.8	43.6	0.7	5.3
20	300.5	0.5	1.3	211.0	0.5	1.7	157.4	0.5	2.2	120.0	0.6	2.7	94.4	0.6	3.2	77.4	0.6	3.7	66.9	0.7	4.2	53.8	0.7	4.8	45.5	0.7	5.3
	312.5	0.5	1.3	219.4	0.5	1.7	163.7	0.5	2.2	124.8	0.6	2.7	98.4	0.6	3.2	80.7	0.6	3.7	69.5	0.7	4.2	56.0 58.3	0.7	4.8	47.4	0.7	5.3
	324.5	0.5	1.3	227.9	0.5	1.7	170.0	0.5	2.2	129.6	0.6	2.7	102.3	0.6	3.2	83.9	0.6	3.7	72.2	0.7	4.2	60.5	0.7	4.8	49.3 51.2	0.7	5.3
	336.6	0.5	1.3	236.3	0.5		176.3			134.4		2.7	-	-		87.1		3.7	74.9		4.2	62.7	_0.7		53.1		
-	348.6	0.5	1.3	244.7	0.5	1.7	182.6	0.5	2.2	139.2	0.6	2.7	110.2	0.6	3.2	90.3	0.6	3.7	77.6	0.7	4.2	65.0	0.7	4.8	55.0	0.7	5.3
	360.6	0.5	1.3	253.2	0.5	1.7	188.9	0.5	2.2	144.0	0.6	2.7	118.0	0.6	3.2	96.8	0.6	3.7	80.2	0.7	4.2	67.2	0.7	4.8	56.9	0.7	5.3
-	-20.0	0.0		200.2	0.0	1.1	.00.0	0.0	2.2		0.0	2.1	110.0	0.0	3.2	30.0	0.0	3.1	00.2	0.7	4.2	07.2	0.7	4.0		0.7	1

Table DV-16 Parabolic Diversion Design Chart (Retardance "D" and "C," Grade 10.00%)

												Grad	e 10.00) Pei	Cent												
Q	v	1=2.0		V1=2.5			٧	1=3.0		V	/1=3.5		V	1=4.0	-	٧	1=4.5		V1=5.0			V	/1=5.5		٧	1=6.0	
CFS	-	-	100	T	D	V2	TI	D	V2	T	D	V2	T	D	V2	T	D	V2	T	D	V2	T	D	V2	T	D	V
-	T	D	V2	9.4	0.5	1.7	6.8	0.5	2.2	5.3	0.5	2.6	4.1	0.6	3.2	3.4	0.6	3.6	2.6	0.7	4.1					100	
5	13.3	0.4	1.3	18.7	0.5	1.7	13.8	0.5	2.2	10.9	0.5	2.6	8.5	0.6	3.2	7.1	0.6	3.6	5.9	0.6	4.1	4.9	0.7	4.7	4.0	0.7	5.
10	26.6	0.4	1.3	28.0	0.5	1.7	20.7	0.5	2.2	16.3	0.5	2.6	12.8	0.6	3.2	10.9	0.6	3.6	9.0	0.6	4.1	7.5	0.6	4.7	6.3	0.7	5
15	39.9 53.2	0.4	1.3	37.4	0.5	1.7	27.6	0.5	2.2	21.7	0.5	2.7	17.0	0.6	3.2	14.5	0.6	3.6	12.1	0.6	4.1	10.2	0.6	4.6	8.5	0.7	5
20		0.4	1.3	46.7	0.5	1.7	34.5	0.5	2.2	27.1	0.5	2.7	21.3	0.6	3.2	18.1	0.6	3.6	15.1	0.6	4.1	12.7	0.6	4.7	10.8	0.7	5
25	66.5	0.4	1.3	56.1	0.5	1.7	41.4	0.5	2.2	32.5	0.5	2.7	25.5	0.6	3.2	21.7	0.6	3.6	18.1	0.6	4.1	15.2	0.6	4.7	12.9	0.7	
30	79.8	0.4	1.3	65.4	0.5	1.7	48.3	0.5	2.2	37.9	0.5	2.7	29.8	0.6	3.2	25.3	0.6	3.6	21.1	0.6	4.1	17.8	0.6	4.7	15.1	0.7	!
35	93.1	0.4	1.3	74.7	0.5	1.7	55.2	0.5	2.2	43.3	0.5	2.7	34.0	0.6	3.2	29.0	0.6	3.6	24.1	0.6	4.1	20.3	0.6	4.7	17.2	0.7	1
40	106.4	0.4	-	84.1	0.5	1.7	62.1	0.5	2.2	48.8	0.5	2.7	38.3	0.6	3.2	32.6	0.6	3.6	27.2	0.6	4.1	22.8	0.6	4.7	19.4	0.7	1
45	119.7	0.4	1.3	93.4	0.5	1.7	69.0	0.5	2.2	54.2	0.5	2.7	42.5	0.6	3.2	36.2	0.6	3.6	30.2	0.6	4.1	25.4	0.6	4.7	21.5	0.7	
50	133.0	0.4	1.3	102.8	0.5	1.7	75.9	0.5	2.2	59.6	0.5	2.7	46.8	0.6	3.2	39.8	0.6	3.6	33.2	0.6	4.1	27.9	0.6	4.7	23.7	0.7	
55	146.3	0.4	1.3	112.1	0.5	1.7	82.8	0.5	2.2	65.0	0.5	2.7	51.0	0.6	3.2	43.4	0.6	3.6	36.2	0.6	4.1	30.5	0.6	4.7	25.9	0.7	
60	159.6	0.4	1.3	121.4	0.5	1.7	89.7	0.5	2.2	70.4	0.5	2.7	55.3	0.6	3.2	47.1	0.6	3.6	39.2	0.6	4.1	33.0	0.6	4.7	28.0	0.7	
65	172.9	0.4	1.3	130.8	0.5	1.7	96.6	0.5	2.2	75.8	0.5	2.7	59.5	0.6	3.2	50.7	0.6	3.6	42.2	0.6	4.1	35.5	0.6	4.7	30.2	0.7	
70	186.2	0.4	1.3	140.1	0.5	1.7	103.5	0.5	2.2	81.2	0.5	2.7	63.8	0.6	3.2	54.3	0.6	3.6	45.2	0.6	4.1	38.1	0.6	4.7	32.3	0.7	
75	199.5	0.4		149.5	0.5	1.7	110.5	0.5	2.2	86.7	0.5	2.7	68.0	0.6	3.2	57.9	0.6	3.6	48.3	0.6	4.1	40.6	0.6	4.7	34.5	0.7	13
80	212.8	0.4	1.3	158.8	0.5	1.7	117.4	0.5	2.2	92.1	0.5	2.7	72.3	0.6	3.2	61.5	0.6	3.6	51.3	0.6	4.1	43.1	0.6	4.7	36.6	0.7	
85	226.1	0.4	1.3	168.1	0.5	1.7	124.3	0.5	2.2	97.5	0.5	2.7	76.5	0.6	3.2	65.2	0.6	3.6	54.3	0.6	4.1	45.7	0.6	4.7	38.8	0.7	
90	239.4	0.4		177.5	0.5	1.7	131.2	0.5	2.2	102.9	0.5	2.7	80.8	0.6	3.2	68.8	0.6	3.6	57.3	0.6	4.1	48.2	0.6	4.7	40.9	0.7	
95	252.7	0.4	1.3	186.8	0.5	1.7	138.1	0.5	2.2	108.3	0.5	2.7	85.0	0.6	3.2	72.4	0.6	3.6	60.3	0.6	4.1	50.7	0.6	4.7	43.1	0.7	
00	266.0	0.4		196.2	0.5	1.7	145.0	0.5	2.2	113.7	0.5	2.7	89.3	0.6	3.2	76.0	0.6	3.6	63.3	0.6	4.1	53.3	0.6	4.7	45.2	0.7	
105	279.3	0.4	1.3	205.5	0.5	1.7	151.9	0.5	2.2	119.2	0.5	2.7	93.5	0.6	3.2	79.6	0.6	3.6	66.4	0.6	4.1	55.8	0.6	4.7	47.4	0.7	L
110	292.6	-	1.3	214.9	0.5	1.7	158.8	0.5	2.2	124.6	0.5	2.7	97.8	0.6	3.2	83.3	0.6	3.6	69.4	0.6	4.1	58.3	0.6	4.7	49.5	0.7	
115	305.9	0.4	1.3	224.2	0.5	1.7	165.7	0.5	2.2	130.0	0.5	2.7	102.0	0.6	3.2	86.9	0.6	3.6	72.4	0.6	4.1	60.9	0.6	4.7	51.7	0.7	
20	319.2	-	1.3	233.5	0.5	1.7	172.6	0.5	2.2	135.4	0.5	2.7	106.3	0.6	3.2	90.5	0.6	3.6	75.4	0.6	4.1	63.4	0.6	4.7	53.8	0.7	
25	332.5 345.8	0.4	1.3	242.9	0.5	1.7	179.5	0.5	2.2	140.8	0.5	2.7	110.5	0.6	3.2	94.1	0.6	3.6	78.4	0.6	4.1	66.0	0.6	4.7	56.0	0.7	
30		-	1.3	252.2	0.5	1.7	186.4	0.5	2.2	146.2	0.5	2.7	114.8	0.6	3.2	97.7	0.6	3.6	81.4	0.6	4.1	68.5	0.6	4.7	58.1	0.7	
35	359.1	0.4	_	261.6	0.5	1.7	193.3	0.5	2.2	151.7	0.5	2.7	119.0	0.6	3.2	101.3	0.6	3.6	84.4	0.6	4.1	71.0	0.6	4.7	60.3	0.7	I
140	372.4	0.4	1.3	270.9	0.5	1.7	200.2	0.5	2.2	157.1	0.5	2.7	123.3	0.6	3.2	105.0	0.6	3.6	87.5	0.6	4.1	73.6	0.6	4.7	62.5	0.7	
145	385.7 399.0	0.4	1.3	280.2	0.5	1.7	207.1	0.5	2.2	162.5	0.5	2.7	127.5	0.6	3.2	108.6	0.6	3.6	90.5	0.6	4.1	76.1	0.6	4.7	64.6	0.7	

RETARDANCE "D" AND "C"

Construction

Prior to start of construction, diversions should be designed by a qualified design professional. Plans and specifications should be referred to by field personnel throughout the construction process. A diversion should be built according to planned alignment, grade and cross section. Typically, a diversion is constructed with the following activities.

Site Preparation

Determine exact location of any underground utilities (see Appendix C: MS One-Call and 811 Color Coding).

Locate and mark the alignment of the diversion as shown on the plans. Minor adjustments to the grade and alignment may be required to meet site conditions. The alignment should maintain a positive grade toward the outlet and end in a stable outlet or an area that can be stabilized.

Clear the construction area of trees, stumps, brush, sod and other unsuitable material which would interfere with compaction of the ridge.

Disk or scarify the area where the ridge is to be installed before placing the fill.

Clean out and refill with compacted earth fill all ditches, swales or gullies to be crossed.

Apply gravel or hard surface protection at vehicle crossings to prevent rutting.

Install stable outlets prior to construction. Adequate vegetation should be established in the outlet channel. If vegetation cannot be established, use *Erosion Control Blankets* and/or *Rock Outlets* or *Outlet Protection*.

Grading

Excavate, fill and shape the diversion to planned alignment, grade and cross section. The channel should have a positive grade toward the outlet to avoid ponding. Where possible, blend diversion into the surrounding landscape.

Overfill and compact the ridge, allowing for 10% settlement. Fill should be placed in lifts of no more than 6" to 8" in depth. Compaction may be achieved by driving wheeled equipment along the ridge as lifts are added. The settled ridge top must be at or above design elevation at all points.

All earth removed and not needed for the practice should be spread or disposed of so that it will not interfere with the functioning of the diversion.

Erosion and Sediment Control

Control sediment along grading limits with sediment control measures.

Leave sufficient area adjacent to the diversion to permit clean-out and regrading.

Immediately after installation, install vegetation treatment or other means to stabilize the diversion in accordance with plans.

Install gravel or hard surface protection at vehicle crossings.

Stabilize diversion outlets in accordance with plans.

Construction Verification

Check finished grades and cross section of diversions to eliminate constrictions to flow. Check all ridges for low spots and stability.

Common Problems

Consult with a qualified design professional if any of the following occur:

Variations in topography on site indicate diversion will not function as intended. Changes in plans will be needed.

Design specifications for seed variety or seeding cannot be met. Substitutions not approved by the design professional could result in erosion and lead to diversion failure.

Seepage is encountered during construction. It may be necessary to install drains.

Maintenance

Inspect weekly and following each storm event for erosion until the diversion is vegetated.

Remove debris and sediment from the channel, and rebuild the ridge to design elevation where needed.

Check diversion outlet for erosion and repair if area becomes unstable. Maintain vegetation with periodic fertilization and mowing to keep vegetation in a vigorous, healthy condition. Mow for weed and brush control during the first year and as needed to prevent brush and tree seedlings from becoming established after the first year of installation.

When the work area has been stabilized, remove temporary diversions, sediment barriers and traps, and repair bare or damaged areas in the vegetation by planting and mulching or sodding.

Stabilize all eroded, rutted or disturbed areas as soon as possible with vegetation or synthetic erosion control measures as specified in the design.

References

BMPs from Volume 1

Chapter 4

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Temporary Seeding (TS)	4-103
Drop Structure (DS)	4-156
Grass Swale (GS)	4-162
Lined Swale (LS)	4-190
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Typical Temporary Erosion Control Measures	4-155
(Temporary Shoulder Berm)	

